OTIC FILE CUPY

DEPARTMENT OF OCEAN ENGINEERING

MASSACHUSETTS INSTITUTE OF TECHNOLOGY CAMBRIDGE, MASSACHUSETTS 02139

REMOVAL OF OUT-OF-PLANE DISTORTION IN MILD STEEL PANELS USING FLAME HEATING

by

Larry Lee Janca

Course XIIIA

Volume 2

DISTRIBUTION STATEMENT A Approved for public release; Distribution Unlimited

AD-A 187 803

This report discusses removed of out of plane distortion in mild steel panels using flame heating. Tables (data), are presented with charts and OF OUT-OF-PLANE DISTORTION IN MILD STEEL PANELS REMOVAL' USING FLAME HEATING bу Н Larry Lee Janca B.S.. University of California (1976)SUBMITTED TO THE DEPARTMENT OF OCEAN ENGINEERING IN PARTIAL FULFILLMENT OF THE REQUIREMENTS FOR THE DEGREE OF S.M., NAVAL ARCHITECTURE AND MARINE ENGINEERING at the MASSACHUSETTS INSTITUTE OF TECHNOLOGY May 1987 Copyright (c) 1987 Massachusetts Institute of Technology dens Se James

Department of Ocean Engineering

May 9 1987

Signature of Author_

Certifited by Koarl Model. Koichi Masubuchi For Professor, Ocean Engineering and Materials Science Thesis Supervisor be .ion Accepted by_ Professor A. Douglas Carmichael Chairman, Departmental Graduate Committee Department of Ocean Engineering ton/

> DISTRIBUTION STATEMENT A Approved for public release; Distribution Unlimited

Availability Codes Avail and/or Special Dist

APPENDIX F

1/8" STIFFENED PLATE OUT-OF-PLANE DEFLECTION READINGS RECORDED AFTER LINE HEATING THE FIRST PASS

Appendix F contains 10 sets of out-of-plane deflection measurements. The 1st set was recorded after welding but prior to any line heating. The rest were taken after each panel was line heated the first time. See Table 2-2 for the 1st pass line heating sequence.

NOTE: In appendixes D, E, F, and G the TRANSVERSE and LONGITUDE spacing is 2 inches. All deflection readings in the matrixes are in .001 inches. For example, the out-of-plane distortion at 10 inches TRANSVERSE and 2 inches LONGITUDE, in the matrix labeled "DISTORTION MEASUREMENTS OF 3/16" PLATE AFTER WELDING" is -0.075 inches (i.e. 0.075 below the reference point). This point is designated D(6,2) as it is on the 6th line in the TRANSVERSE direction and the 2nd line in the LONGITUDE direction.

COLEMPTICAL CONTROL CONTROL OF THE SAME AND THE SAME AND THE SAME CONTROL OF THE SAME

DISTORTION MEASUREMENTS OF 1/8" PLATE AFTER WELDING

TRANSVERSE

			0	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
		0 ¦	-131	 _	-119				-108		-110		-107		-95		-107	-109	-110		-123
			-101			-130 -146			-74			-84 -58			-49			-104 -89			-73
		6;				-153			-/4			-30 -46			-47			-67			-/3
		B :				~144			-45			-42			-16			-49			-32
	1					-128						-32			••			-38			JL
	1			-109	-124			-60	-21	-15	-14		-9	-1	10	-10	-20		-19	-12	7
	1					-114						1						-8	•		-
	1 1	6 :	-70			-106			4			15			34			-1			40
	1	8 ;				-96						36						7			
			-67			-85			15			53			53			31			69
	2					-57						58						69			
			-65.		-35	-18			28		45	57	68		80		87	93	104		105
	2					-60						44						74			
	28					-88			37			32			99			69			114
	3					-88			٠,			12						71			
	32		-69			-76			36			-3			95			70			129
	3		75	7,	74	-63		_	38	• ,		-3	24	17	4.00	07	0.4	77	4.84		171
	1 3			-/6	-/1	-53 -43	-2/	5	30	16	1	0 7	24	63	102	93	90	91	101	115	134
	: 31 : 4(-45 -45			32			19			102			96 91			175
	42		-03			-59			34			33			102			91			135
			-101			-71			27			35			102			96			133
	. 4		101			-69			21			28			102			97			133
			-121		-77	-59	-39		6		20	34	46		89		107		119		142
	: 50				• • •	-108	٠.		•			40	,,,					97	•••		• '-
			-139			-145			-9			38			80			78			121
	5					-167						24						55			
			-166			-186			-35			11			80			39			111
1	5	3 ;				-204						-5						33			
;	60)	-195	-214	-224	-215	-184	-133	-65	-58	-46	-29	-10	12	41	22	16	19	37	63	96
	62					-222						-44						3			
			-227			-239			-96			-50			18			-3			79
	66					-253						-57						-2			
			-265			~253			-131			-73			-5			-5			57
	70					-245						-88						-7			
,	72	? ;	-301		-259	-234	-212		-169		-126	-109	-87.		-45		-18	-1	13		33

THE STATE OF THE S

DISTORTION MEASUREMENTS OF 1/8" PLATE AFTER PANEL 5 WAS LINE FLAME HEATED FOR THE FIRST TIME

	JERSE

		()	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
	0	-161			-150	-154	-150		-139		-140		-137		-126		-137	-140	-139		-152
	2	!				-162						-115						-135			
	4	-142				-179			-108			-91			-82			-121			-105
	6	!				-188						-80						-100			
	8	-126	,			-180			-82			-76			-50			-83.			-66
1	10	1				-168						-67						-73			
1	12	-114	-1	44	-162	-162	-139	-99	-59	-51	-49	-47	-43	-36	-27	-49	-60		-57.	-48	-27
1	14	ŧ.				-159						-33						-50			_
•	16	: -104	١			-151			-36			-16			-4			-44			5
1	18	t i				-143						2						-37			
	20	-103	;			-131			-27			17			12			-11			33
•	22	1				-100						18						27			
	24	-104	•		-74	-60	-40		-17		1	13	24		37		46		65		68
	26	1				-104						18						35			
	28	-104	•			-138			-8			20			54			28.5			77
	30	1				-139						7						30			
3	32	-108	}			-122			-10			-5			50			32			91.5
	34					-101						-4						44			
	36	-115	-1	13	-104	-85.	-62	-36	-8	-7	-5	0	13	33	57	57.5	61.5	65	73	82	99
	38					-71.						8						70			
	40	-125	i			-73			-12			22			57			62			100
•	42	!				-91						36						58			
ı	44	-140)			-107			-16			28			60			60.5			100
	46					-107						4						61			
	48	: -15	3		-116	-99	-79		-36		-22	-8	5		49		69		83		110
	50	;				-153						-2						59			
•	52	: -177	7			-193			-52			-3			42			41			90
	54	1				-216						-15						18			
		: -20	3			-235			-75			-25			44			2			83
	58					-251						-41						-4			
		-23) -:	252	-265			-172	-101	-93	-80	-63	-43	-22	7	-11	-20	-15	4.5	34	70
	62					-265						-78						-29			
		· 1 -25	Q			-277			-130			-81			-11			-33			53
	66		•			-288						-88						-30			
		-29	Q			-287			-163			-102			-34			-31			34
	70					-277						-116						-31			
		: -33	5		_201	-264			-199		-154		-115		-71		-41	-24	-10		14
	12	-33	J		-270	201	474		477		137	130	-10				•				

CONTRACTOR DESCRIPTION OF CONTRACTOR PROCESSES AND PROCESS

TRANSVERSE

		0	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
0	:	-147		-136	-140	-135		-125		-128	-128	-125	-125	-115		-125	-127	-128		-140
2	į	-139			-152			-111			-103			-85			-122			-112
4	!	-135			-174			-99			-80			-70			-108			-90.
6	1	-129			-191			-90			-70			-57			-85			-69
8	1	-125			-191			-76			-68			-41			-68.			-48.
		-123			-185			-65			-60			-28			-56			-30
12	1	-121	-156	-182	-182	-155	-107	-57	-47	-44	-42	-37	-29	-18	-37	-46	-48	-40	-30	-10
14	1	-123			-181			-52			-28						-34			8
16	ŀ	-118			-171			-38			-12			4			-30			24
18	!	-120			-156			-31			9			13			-23			39
20	1	-122			-139			-33.			23.5			19			3			54
		-126			-111			-29			21			37			42			64
			-115	-92	-74	-51	-37	-26	-14	-2		26		44	55	59		82		90
		-127			-106			-21			17			50			49			96
		-127			-128			-17.			18.5			61			44			99
		-130			-132			-18			2			60			47			106.
		-131			-127			-17.			-13			57			48.5			113
		-131			-114			-16	_		-10			62			61			116
			-128	-116	-95		-40	-14	-9	-6	0	17	38	64	68	74	80	91	102	120
		-138			-73			-17			13			65			84			121
		-141			-66			-16			31			66			76			121
		-146			-78			-11			47			67			73			120
		-152			-94			-18.			37			69			<i>7</i> 5.5			121
		-157			-101			-26			10			65			78			125
		-166		-122	-103			-35	-27	-18	-3	13		60		83		101.		131
		-171			-155			-34			6			67			76			117
		-179			-193			-45			7			55			38			111
		-189			-216			-56			-4			49			35			110
		-200			-233			-66			-13			58			20			103.
		-213			-248			-77			-28		_			_	14			99
			-245	-259	-253	-219	-164	-91	-81	-68	-50	-29	-7	23	4	-3	_	24	54	90
		-236			-257			-101			-63			14			-12			83
		-251			-267			-117			-66			4			-16			73
		-264			-276			-134			-72			-8			-12			65
		-282			-273			-147			-85			-16			-13.			53
		-298			-261			-166			-98.	_		-32			-14	_		42
72	ļ	-305		-271	-245	-223	-201	-180		-135	-118	-96		-52		-23	-4	8	22	31

SOOM PERSONAL REFERENCIA AND THE CONTROL OF THE PROPERTY OF THE CONTROL OF THE PROPERTY OF THE

DISTORTION OF 1/8" PLATE AFTER PANELS 5. 4. AND 6 WERE LINE FLAME HEATED FOR THE FIRST TIME

			0	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
	; 1	0 :	-145		-134	-138	-133	-128	-122		-126	-127	~122		-111		-122	-125	-126	-129	-138
			-136			-150			-109			-101			-84			-120			-110
			-132			-172			-97			-77			-68			-117			-89
			-126			-187			-88			-67			-55			-88			-68
			-123			-187			-74			-66			-39			-72			-49
			-121			-182			-64			-58			-25			-64			-31
			-118	-153	-180			-105	-56	-46	-42.	-41	-37	-28	-18	-39	-51	-54	-47	-34	-11
			-120			-178			-51			-26.			-4			-40			6
			-115			-169			-37			-12			3			-31			21
			-117			-153			-30			12			12			-20			35
			-118			-137			-32			26			17			7			49
			-124			-109			-28		_	22			34			42.5			60
			-123	-111	-90	-72		-35		-12	-3		25	38	41	50	55	66	77	86	86
			-125			-105			-20			16			48			60			92
			-125			-125			-16			16			60			60.5			95
			-127			-130			-17			-3			60			61			104
			-128			-124			-16			-18			58			57.5			111
			-129	407	444	-111	,,	70	-15		-	-14		70	63			64			115
			-133	-126	-114		~66	-38	-13	-8	-7	-	15	39	66	70	75	80	90	102	
			-126			-71			-15			15			68			85			122
			-140			-64			-14			36			70			81			124
_		-	-145			-77			-9			53			71			83			124
			-151 -156			-93 -99			-16 -22			43			74			91			126
			-165	- 1 45	121		00				4.	15	40		71			91.5	444	400	134
			-171	-145	-121	-153	-00		-31. -30	-22	-14		18		66	80	90	101	110	122	140
			-179			-192			-42			13 14			74 64			88 70.5			127 124
			-190			-215			-51			5			59			47			124
			-201			-231			-62			-4			69			33			120
			-214			-245			-72			-19			50			27			116
			-225	-245	-258		-217	-158	-85	-74	-60	-40	-20	4	35	17	10	16	39	71	109
			-238	- 10	200	-255			-95	′ '	•	~53		•	30	• (10	4	37	′.	104
			-251			-266			-111			-54			19			1			96
			-268			-275			-126			-60			8			7.5			89
			-284			-271			-140			-73			1			8			79 . 5
-			-300			-259			-158			-85			-14			10			70
			-318		-272	-244	-220		-170		-124		-79	-58	-32		0.5	21	34	50	60
'		•			_, _		~					- • •	• •	~	72		4.0	~ *	J7	30	20

A COMPANY OF COMPANY ASSESSMENT OF THE SERVICE OF T

DISTORTION OF 1/8" PLATE AFTER PANELS 5,4,6,AND 2 WERE HEATED THE FIRST TIME

TRANSVERSE

			0	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
•	0	i	-138		-127	-132	-128	-122	-118		-122	-123	-119	-117	-107		-119	-121	-121	-125	-133
	2	;	-130			-145			-106			-91			-80			-117			-106
	4	i	-126			-168			-92.			~65			-66			-105			-86
	6	¦	-121			-186			-85			-55			-53			-85			-65
	8	ļ	-117			-186			-71			-54.			-37.			-71.			-46
			-115			-181			-61			-47			-24.			-63			-28
	12	ŀ	-112	-149	-177	-179	-152	-103	-53	-39	-32	~29	-26	-22	-16	-39	-52	-56	-47	-33	-9
			-115			-177						-13			-10			-43			9
	16	ł	-110			-166			-36			7			4			-34			23
	18	1	-112			-152			-28			33			13			-22			36
	20	ŀ	-114			-135			-31			49			18			5			50
	22	;	-120			-107			-26			39			34			42			60
	24	!	-120	-109	-87	-70	-48	-34.	-23	-11.	-3	11	25	38	42	51.5	56	65.5	78	88	87
	26	ł	-120			-103			-19			21			50			60			92
	28	ŀ	-121			-124			-14.			21			60			60			95
	30	ł	-124			-130			-16			3.5			60			60			104
	32	ŀ	-124			-124			-15			-8			59			56.5			111
	34	1	-126			-111			-12.			-10			64			63.5			115
	36	ŀ	-130	-123	-111	-90	-63	-35	-10	-7	-5	0	16	40.5	67.5	71	76	80	91	103	121
			-134			-68			-12.			15			70			86			
			-136			-60.			-11			37.5			71			83			124
			-141			-73			-5			54			74			85			125
	44	1	-148			-88.			-13			45.5			76			92.5			127
			-152			-95			-19			18			73			95			133
	48	ŀ	-161	-140	-117	-97	-76		-28.	-20	-11	5	21		68.5	81	92.5	102	112		141
	50	ł	-167			-149			-28			14			76			89			129
			-175			-187			-39			16			65			73			125
			-185			-210			-48			6			60			50			125
			-196			-226			-58			-2.5			71			35			121
	58	ł	-208			-240			-69			-16			51			30			118
	60	1	-220	-241	-253	-246	-212	-154	-81.	-71.	-55	-37.	-15	7.5	38	21	14	19	42	74	110.
	62	ŀ				-249			-91			-50			31			7			106
	64	;	-247			-259			-106			~52			22			4			98
	66	ţ	-262			-268			-121			-57			11			10			92
	68	;	-280			-264			-135			-70			4			11			82
			-295			-252			-154			-82			-11			13			72
	72	:	-312	-286	-265	-236	-213		-164		-118	-100	-76	-55	-28		4	23.5	39	54	64

DISTORTION OF 1/8" PLATE AFTER PANELS 5,4,6,2, AND 8 WERE HEATED THE FIRST TIME

TRANSVERSE

				0	2	4	 6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
	ļ	0	;	-132	-124	-122	-126	-122	-117	-111		-116	-117	-113	-111	-101		-113	-116	-116	-120	-128
	i			-125			-140			-100			-85			-78			-112			-102
	ļ			-120			-163			-87			-60			-61			-101			-82
	!	6	ł	-115			-180			-79			-50			-50			-82			-63
	ŧ	8	ł	-111			-180			-66			-50			-33			-69			-44
	ŀ	10	ł	-109			-176			-56			-43			-20			-62			-28
	ľ	12	ţ	-108	-143	-171	-174	-147	-98.	-49	-35	-28	-25	-22	-18.	-14	-37	-50	-54	-45.	-32	-8
				-109			-172			-44			-9			-7			-41			8
				-103			-162			-30			10			6			-33			22
				-105			-147			-25			36			14.5			-21			35
				-108			-131			-27			51			19			5			48
				-113			-102			-23			41			36			41.5			58
				-112	-101	-80	-64.	-44	-30	-20	-8	0	13.5	26		42	51	55.5		76	85	83
				-113			-98			-15			22.5			49			59			88
				-113			-119			-11.			22.5			60			57			91
				-116			-125			-13			4			60			57			99
				-116			-119			-12			-12			57			53			106
				-118	447	4.85	-105	FA	70	-10	_		-10	4.5	70	62			60.5	ae -		109
					-116	-103		-37	-32	-8	-5	-4	0	15	39	65	68	72		85.5	98	114
				~125			-62			-10			14			67			81			116
				-127			-55			- 9			35			69			78			113
				-132			-68 -84			-4			50			70			78.5			116
_				-138 -144						-11			40			72			85			118
					-132	111	-91 -07	- 77		-18 -28	-20		13.5	10		69	75	05	85	100		125
				-160	-132	-111	-73 -144	-/3		-28	-20	-12	3 18	18		63	75	85		102.		130
				-168			-179			-26 -39			29			69 58.5			80.5 65			116 111
				-179			-201			-49			26			54			42			111
				-189			-217			-58.			21			63.5			26			
				-201			-230			-70			8.5			43			20			106 102
					-233	-244		-203	-149		~57	-34		1.5	12	30	11	3.5		29.5	59	95
				-225	200		-240		• 17	-92	0 / •	51	-27	1.0		23	••	7. 7	-5	27.0	3,	89
				-239			-253			-107			-32			13			-7			80
				-253			-263			-122			-41.			3			-2			73
				-271			-261			-136			-60			-5			-2			63
				-285			-248			-154			-81			-20			-1			53
				-302				-212				-123		-83	-63	-38		-10	8	20	35	43
		_	-													-		- 4	J		~~	,,,

STAND PROCESS ASSESSED FRANKS TO STAND SERVICES SERVICES RECESSES AND PROCESSES AND PR

DISTORTION OF 1/8" PLATE AFTER PANELS 5,4,6,2,8, AND 3 WERE HEATED THE FIRST TIME

TRANSVERSE

			0	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
:	0	!	-124		-113	-118	-114	-109	-104		-110	-111	-107	-106	-96		-108	-110	-110	-113	-120
	_	-	-114			-131	•		-91			-79			-71			-96			-98
	_		-111			-155			-81			-51			-57			-75			-80
			-105			-172			-72			-41			-46			-47			-62
1	8	ţ	-101			-172			-60			-42			-31			-28			-44
1	10	ļ	-100			-166			-50			-36			-19			-18			-28
	12	ţ	-97	-133	-161	-164	-139	-91.	-44	-29.	-23	-19.	-17.	-15	-11	-6.5	-2	-5	-10.	-18	
;	14	1	-99			-161			-38			-5			-6			10			5
	16	•	-94			-152			-26			12			6			15			18
			-96.			-137						37			15			18			32
			-99			-121			-22			53			19.5			33			46
			-104			-94	77	27	-17	7 5		44	20	41	35 43	51	65	54 64	75	84	58 84
			-103	-93	-/3	-57	-3/	-23		-3.5	5		29	41		31	03	55	/ 3	70	89
			-104			-91			-10			26			49 60.5			54.5			92
			-105			-112			-6 -7			24.5 5			60.3			55			101
			-107			-117 -112			-, -6			-13			58.5			54			108
			-108 -110			-98			-5			-10.			64			62.5			112
			-114	_100	-97		-51	-25	-2.5	-1 5	-4	0	15	40	67	73		81.5	92	103	118
			-118	100	"	-55	JI	20	-5	1.0	,	16			69.5			88			120
			-121			-48			-4			38			71			84			121
			-127			-61.			1			55			73			85			121
			-133			-79			-6			46			76			91			123
_			-138			-86			-13			18.5			73			91			130
			-147	-126	-105	-87	-67		-22.	-14	-7	8	23		68	81	90	100.	109		137
	50	;	-152			-131			-21			25			76			88.3			125
	52	ł	-161			-174			-32			36.5			66			73.5			122
	: 54	1	-172			-195			-42			34			61.5			51			121
	56	!	-183			-209			-52			29			72			35			116.
			-195			-224			-62.			15.5			52.5			29			113
	60	¦	-207	-227	-238			-143	-75	-50	-26.	-6	10	21.5	39	21	13	18	39	69	_
			-220			-232			-85			-19			33			7			100
			-233			-247			-100			-23.			24			3			92
			-249			-257			-115			-33			12			9			85
			-267			-255			-130			-52			5			10			<i>7</i> 5
			-282			-243			-147			-71	77		-10		2	11	77 F	¥D.	65 57
	1 72	;	-301		-254	-227	-204	-182	-124		-114	-96	-73		-28		2	21	33.5	48	ار

DISTORTION OF 1/8" PLATE AFTER PANELS 5,4,6,2,8,3,AND 1 WERE HEATED THE FIRST TIME

TRANSVERSE

			0	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
		0 :	-76		-78	-89	-90	-90	-88		-96	-98	-95	-94	-85		-98	-100	-101	-104	-111
		2 ;	-76			-100			-78			-66			-60			-86			-89
	-	4	-81			-130			-68.			-38			-47.			-64			-69
	۱ ،	6 :	-81.			-160			-63			-28			-33			-36.			-50
	: {	8 1	-86			-176			-53			-30.			-22			-17			-33
	1	0 ¦				-185			-45			-24			-10			-7			-17
1	12	2 1	-92	-141	-184	-192	-157	-92	-40	-17	-6	-4	-6	-6	-3	1.5	8	6.5	3	-4	3
	1		-98			-188			-37			13			2			19			18
ŀ	16	5 ;	-97			-165			-24			33.5			14			23			33
			-100			-134			-19			60			23			26.5			46
			-104			-110			-23			73			28			42			60
			-108			-84			-18			55			44			64			71
			-105		-74	-59	-35.	-24	-16	-3	7		34	47	50	60	66	75	89	99	98
			-103			-89			-10			25			58			68.5			104
			-101			-108			-4.5			22.5			68.5			68			107
			-101			-109			-4			-1			68.5			70			116
			-100			-99			-2			-20			67.5			69			123
			-99			-83			2			-16.	4.		73			78			126
			-101		-81	-63	-37.	-15		4	-1.5	0	18	47	77	84	91	96.5	104.	116	131
			-103			-41			3.5			21			80			101			133
			-104			-34			6			49			82			96			133
			-108			-47.			13			68.5			84			96.5			133
			-113			-64			7.5			60			88			102.			134.
			-117			-68			2	_		33.5			86			102.			141
			-125	-104	-84	-67	-48		-6	2	8		37.5		81	93	102.		119.	130	147
			-128			-116			-3.5			40			89			99			133
i			-135			-151			-14			53			80			85			129
			-144			-170			-21			51			75 00			63			129
			-152			-184			-30			47			88			48			124
			-163 -173	- 104	_207	-196 -201	_140	_117	-39 -50	-26	-3	35.5 15	29	39	68 54	74	27.5	42.5	52	80	119. 112
i				-174	-20/		-107	-113	-59	-20	-3		21	37		30	2/ . J		JZ	OV	
			-183 -196			-203 -214			-73			2 -2			48 40			19 16			106 98
			-207			-223			-86.			-10			30						_
			-207 -225			-218			-99			-28			23			21.5 21.5			91 80
			-238			-204			-115			-46.			23 9			22.5			70
			-252		_212		-144	-147			-86	-70	-50	-32	-8.5		14	32.5	42	55	61
	' / '	ا ک	-232		-212	-10/	-100	17/	123		-00	-/0	- 30	-32	0.5		10	JŁ.J	74	JJ	91

DISTORTION OF 1/8" PLATE AFTER PANELS 5.4,6,2,8,3,1,AND 7 WERE HEATED THE FIRST TIME

TRANSVERSE

				0	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
	:			-56		-58	-67	-67	-66	-64		-71	-73	-70	-68.	-59		-71.	-74	-74	-77	-85
	ŀ	2	ŀ	-56.			-78			-56			-41			-35			-61			-62
	!	4		-61			-108			-46.			-15			-23.			-40			-46
	;	6		-63			-139			-42			-7			-14			-14			-28.
	!	8		-66			-155			-32			-10			0			5			-12.
		10		-69			-164			-25	_		-5			10.5			14			2.5
		12			-122	-166	-174	-139	-74	-21	3	13		13.5	13	15	20	25	24	19		19
				-78.			-171			-17			32			19.5			36			33.5
		16		-76			-148			-6			52			30			38.5			47
		18		-80			-118			-2			77.5			37			39			59
		20		-83			-93			-6			90			40			53			71
		22 24		-87	75	57	-67 -42	20	-8.5	-3	10	10	69	45	FO	56	70	74	74	07.5	101	80
				-83	-75	-57	-42 -71	-20	-0.1	-1 3.5	10	17	31.5	45	58	61	70	74		96.5	106	106
		26 28		-81 -79			-/1 -89			3.J 9			36 31			67 77			75.5 76.5			111
		20 30		-78			-90			8												112
				-76 .			-80			9			2 -21			76 73			77.5			119
		34		-75			-65			12			-18			73 78			75 82.5			124
I				-76 .	-72	-44	-47.	-25	-3.5		9	۸	0	18	48	81	87		96	105		126. 130
-		38		-78	/ -	7	-30	23	3.3	13	,	V	28.5	10		82.5	07		98.5	IVJ		129.
				-79 .			-27.			14.5			62			84			91			127.
		42		-83			-42			21			85			85			92			126.
				-88			-55			15			72.5			88			96			126
-				-91.			-56			9.5			39			85			96			131
		48		-99		-65	-52.	-37		2	8	12	26	39		79		97		110	118	
				-103			-97.	•		6	_		45			83			90			118
				-107			-133			-3.5			63			76			73			110
				-112			-156			-9			65			71			49			107
				-119			-189			-16			64			81			32			100
				-124			-198			-23			55.5			62			24			93
					-164	-197	-203	-168	-102	-32	-3	20	35	41	41	49	23	10.5	11	28	52.5	83
				-133			-199			-37.			22			43			-2.5			74
				-138			-197			-48.			20			35			-7			62
				-143			-186			-59.			11			24			-2			52
				-152			-164			-69			-9			17			-3			39
				-156			-141			-81			-31			2			-3.5			25
	:	72	ł	-163		-141	-126	-114	-102	-90		-64	-55	-41.	-31	-15		-4	5	8	13	13.5

DISTORTION OF 1/8" PLATE AFTER PANELS 5,4,6,2,8,3,1,7,AND 9 WERE HEATED THE FIRST TIME

TRANSVERSE

											HIMM) 4 E (10)	-								
			0	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
ł	0	;	-44		-45.	-54.	-55	-53.	-51		-58	-59.	-56	-55	-46		-57	-60	-60	-63	-70
!	2	ŧ	-45			-66.			-43			-29			-22			-47			-49
ţ	4	í	-50.			-96.			-34.			-2			-10			-27			-32
;	6	1	-53			-127			-30			5.5			0			-1.5			
;	8	1	-57			-144			-21.			1.5			12.5			17.5			1.5
ţ	10	ŀ	-61			-154			-14			7			23			26			16
ţ	12	ŧ	-64	-113	-158	-165	-130	-65		13	23	26	24	24	27	31	36.5		32	25	33
ł	14	ł	-70.			-164			-9			44			31			47			47
1	16	ł	-69			-142			2.5			63.5			41			50			60
¦	18	ł	-73			-111			7			89			46			51			72
-	20	1	-76			-87			1.5			100			50			64			84
1	22	1	-82			-61			5			78.5			65			85			94
¦	24	1	-78	-70	-51	-35.	-14	-3	6	17	26.5		52.5	65	70		84	95	108	118	119
ł	26	1	-76			-66			11			43			75			86			123
L¦	28	į	-74.			-84			14.5			36			85			87			124
0 ;	30	ļ	-74.			-85			13.5			5			83			89			132
N :	32	ŧ	-73			-75			14.4			-20			79			88			136
G	34		-73			-60.			16.5			-18			84			95	445	404	138
I	36	1	-74.	-70	-61		-22	-1		11.5	1	_	19	51	86	74	102		115.	124.	140
T			-76			-27			16			30			87			108			140
U ¦			-79			-25			17			65			88			97			139
D :			-82			-40			23			88			88			93			136
	44		-88			-55			17			75			91			96			135
- 1	46		-92			-56			11			41			88		4.5	96.7	4.15		140
¦			-101	-85	-66				2		14		40		81	93	100		115		141
			-105			-98			6			47			87			106			122
			-110			-134			-4			65			77			103			116.
			-117			-157			-10			68			72			83			112
			-123			-180			-17			68			82			63.5			106
			-129			-201			-25		20 5	58			62	70	20 E	50	44 6	/5	99
					-202	-206		-106			22.5			45.5	50	ახ	28.3		44.5	65	89
			-139			-205			-41			29			43			12.5			82
			-146			-202			-51			29			36			11			72 /5
			-152			-194			-62			20			25			23.5			65 54
			-161			-171			-72			-4 20			20 5			24 17			54 43
			-166			-148		4.0.	-85		,,	-28		_ 20	-10					31	43 34
	72	! !	-172		-149	-132	-120	-109	-75.		-65	-55	-40	-28	-10		4	16.5	22	21	34

APPENDIX G

1/8" STIFFENED PLATE OUT-OF-PLANE DEFLECTION READINGS RECORDED AFTER LINE HEATING THE 2ND, 3RD, AND 4TH PASS

Appendix G contains 8 sets of out-of-plane deflection measurements. The first 4 are for the 2nd heating pass, the next 2 are for the 3rd pass, and the last 2 are for the 4th pass. See Table 2-2 for the line heating sequence of each pass.

NOTE: In appendixes D, E, F, and G the TRANSVERSE and LONGITUDE spacing is 2 inches. All deflection readings in the matrixes are in .001 inches. For example, the out-of-plane distortion at 10 inches TRANSVERSE and 2 inches LONGITUDE, in the matrix labeled "DISTORTION MEASUREMENTS OF 3/16" PLATE AFTER WELDING" is -0.075 inches (i.e. 0.075 below the reference point). This point is designated D(6,2) as it is on the 6th line in the TRANSVERSE direction and the 2nd line in the LONGITUDE direction.

SECURIOR REPORTS RECEIVED

ECOCCI - PSECOCCI - SSSSSSSS - ECOCCI -

DISTORTION OF 1/8" PLATE AFTER PANEL 5 WAS HEATED THE SECOND TIME

TRANSVERSE

) 2		6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
;	0	-141			-153			-149			-159			-146			-161			-172
1	2	;			-164						-128						-148			
;	4	;			-196						-102						-126			
¦	6	!			-227						-96						-98			
;	8	!			-245						-100						-79			
;	10	!			-257						-94						-70.			
1	12	: -162	-213	-259	-268	-233	-165	-112	-87	-76	-75	-77	-78.	-76	-70	-63	-62	-65	-73.	-69
;	14	:			-266						-57						-53			
;	16	!			-245						-38						-53			
ŀ	18	1			-215						-15						-54			
¦	20	<u> </u>			-190						-7						-42			
į	22	!			-164						-31						-21			
1	24	1 -179)		-138			-98			-65			-35			-8.5			16.5
1	26	1			-167						-46						-10			
L	28	!			-184						-26						-4.5			
0	30	!			-185						-27						2.5			
	32				-176						-31						1			
	34				-163						-18						3			
1 :	36	-176	-172	-164	-148	-127	-106	-85	-44	-11	0	-5	-16	-19	-6.5	6		18	24	38
T	38	;			-132						14						10			
U	40	1			-127						26						-1			
D :	42	1			-140						24						-6			
E	44	1			-154						-10						-5			
1	46	1			-156						-58						-8			
1	48	: -201			-154			-101			-77						4			39
	50				-201						-59.			-24			11.5			
	52				-239						-43						33			
	54	1			-264						-43						47			
	56				-285						-46						57			
	58				-304						-59			٠.		-	59			4.7
		1 -23	2 -269	-303			-207	-137	-112	-91		-75	-72	-56	-35.	3		51	31	-17
	62				-305						-89						1			
	64				-303						-86						-27			
	66				-293						-91						-45			
	68				-271						-111						-67			
	70		_		-248						-134						-87			
1	72	-26	}		-233			-196			-160			-117			-94			-77

SECONOMISSOS DE SESSES EN PROPERTIES DE SECONOMISSOS DE LA PROPERTIE DE COCOCOCO DE LA POPULA DE COCOCOCOCOCOC

DISTORTION OF 1/8" PLATE AFTER PANELS 5 AND 4 WERE HEATED THE SECOND TIME

TRANSVERSE

												•								
		0	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
	0	: -127			-139			-136			-146			-133			-148			-158
	2				-151						-116						-135			
ļ	4	-			-182						-91						-115			
	6	1			-213						-84						-87			
1	8	!			-231						-89						-69			
	10	1			-243						-83						-60.			
		-148	-199	-246			-155	-101	-76	-65	-63	-65	-68	-66	-61	-54	-54	-57	-65	-60
	14				-255						-45						-45			
	16				-236						-26						-46			
	18				-206						-4						-48			
	20				-182						3						-35			
	22				-155						-21						-15			
1	24	-164			-127			-88			-57			-28			-3			21
	26				-153						-40						-6			
	28				-164						-23						0			
	30				-156						-28						7			
	32				-141						-34						5			
	34				-124						-20						8			
		-162	-150	-131			-83	-78	-39	-10		-4	-14	-15	-3	9	5.5	19	23.5	37.5
	38				-96						18						11			
	40				-97.						32						-2			
D	42	1			-116						31						-8			
	44				-136						-4						-7.5			
	46	_			-143						-54						-11			
- 1	48	-183			-143			-93			-74			-24			0			32
	50	:			-191						-55						7			
	52				-228						-37						28			
	54				-251						-36						41			
1	56	!			-271						-40						50			
	58				-288						-54						51			
		-209	-247	-283		-258	-194	-127	-103	-86		-73	-72	-57.	-39	-2		41	19	-30
	62				-285						-88						-6			
	64				-282						-84						-35			
	66				-272						-88						-54			
	68				-250						-108						-77			
	70				-227						-130						-99			
		-240			-211			-182			-155			-122			-107			-100
•	, _	. 4.1V						102									44,			

DISTORTION OF 1/8" PLATE AFTER PANELS 5,4, AND 1 WERE HEATED THE SECOND TIME

TRANSVERSE

			0		2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
1	0	:	-128				-141			-139			-148			-135			-151			-161
	2						-144						-117						-138			
:	4	:					-167						-92						-117			
	6	;					-199						-86						-90			
i	8	1					-218						-92						-71			
1	10	¦					-231						-87						-63			
	12	1	-154	-19	5	-233	-238	-206	-148	-106	-81	-69	-67	-69	-71	-69	-64	-57	-56.	-59	-62.	-62
	14	ŀ					-228						-49						-48			
	16	;					-198						-29						-49			
;	18	ļ					-166						-6.5						-51			
i	20	;					-150						0						-39			
	22						-138						-25						-18			
			-170				-132			-93			-61			-31			-6.5			17.5
	26						-156						-44						-10			
	28						-166						-28						-2			
	30						-159						-32						5			
	32						-145						-35						2.5			
	34						-130						-21						4			
			-167	-15	i4	-136		-9 7	-87.	-82	-41	-11		-4.5	-16.	-18	-6	6	11	16	21	35
	38						-101						16.5						7			
	40						-101						30						-5			
	42						-120						28						-10			
	44						-140						-6						-10			
	46						-146						-56			•			-13			~~
			-184				-146			-96			-76.			-26			-2			30
	50						-194						-58						6			
	52						-230						-40						27			
	54						-254						-38.						40			
	56						-273						-42						49			
	58		244			200	-291	2/4	10/	400	4 85	00	-56.	. 7/	. 75	_21	_41	_4	50	70	17 5	-72
			-211	-24	H	-280		-260	-140	-129	-105	-86		-76	-/3	-61	-41	-4		37	17.5	-32
	62						-288						-89						-8 05			
	64						-284						-86						-38			
	66						-275						-91						-56			
	68						-251						-109						-79 -101			
	70		_047				-228			_104			-131			_125			-101			_101
i	12	i	-243				-213			-184			-158			-125			-109			-101

DISTORTION OF 1/8" PLATE AFTER PANELS 5,4,1, AND 7 WERE HEATED THE SECOND TIME

TRANSVERSE

												_								
		0	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
	0	l -131			-145			-141			-151			-138			-153			-162
	2				-147						-121						-140			
ļ	4	!			-170						-94						-119			
;	6	1			-202						-88						-92			
;	8	:			-221						-94						-74			
	10				-234						-89						-66			
		-156	-198	-236	-240	-209	-150	-108	-83	-71.	-70	-72	-73.	-71	-66	-59		-62	-70	-65.
	14				-230						-51						-50			
	16				-201						-31						-52			
	18				-169						-9						-54			
	20				-152						-2						-42			
;	22	į .			-140						-26.						-21			
!	24	-172			-134			-95			-63			-34			-9			15
	26	1			-158						-46						-11			
L	28	-			-169						-29						-5			
0 :	30	1			-162						-31						2			
N :	32	!			-148						-34						-1			
G	34	1			-132						-20						1			
1 :	36	-169	-156	-138	-117	-100	-90	-84	-43	-11	0	-4	-18	-21	-9.5	2	8	13	18	31
T :	38	1			-103						16						4			
U :	40	}			-102						28						-8			
D :	42	!			-119						25						-14			
E	44	!			-138						-10						-13			
1	46	}			-145						-59.						-16.			
¦	48	-188			-148			-99			-79			-29			-5			25.5
1	50	:			-178						-59						2			
;	52	!			-203						-40						23			
	54	1			-222						-39						37			
;	56				-248						-44						46			
1	58	1			-274						-59						47			
1	60	-212	-247	-279	-286	-255	-194	-132	-108	-91	-82	-78	-77	-63	-44	-7	25	37	14	-36
1	62	:			-284						-91						-12			
:	64	:			-278						-87						-41			
ļ	66	Į.			-264						-90						-59			
	68	!			-240						-110						-82			
	70				-221						-133						-104			
		-241			-214			-186			-159			-126			-111			-105

DISTORTION OF 1/8" PLATE AFTER PANEL 1 WAS HEATED THE THIRD TIME

TRANSVERSE

	0	2		_						18									36
: 0:	-131			-145						-154						-156			-166
1 2 1				-143						-122						-143			
1 4 1				-161						-95						-123			
1 6 1				-185						-88						-95			
8 1				-198						-94						-77			
1 10 1				-204						-89						-70			
1 12 1		-185	-206			-132	-111	-85	-72	-70	-72	-75	-74.	-69.	-63	-63	-66	-72	-68.
1 14 1				-186						-52						-55			
16				-156						-33						-56			
18 1				-134						-12						-57			
1 20 1				-129						-6						-44.			
1 22 1				-130						-30						-23.			
1 24 1	-174			-137			-98.			-66			-36			-12			12
1 26 1				-162						-49.						-14			
28 1				-174						-32						-8			
: 30 :				-167						-33						-2			
1 32 1				-153						-34						-5			
1 34 1				-136						-19						-3			
1 36 1		-159	-140	-120	-103	-93	-88	-45	-11	0	-5	-19.	-23	-12.	-1	4	9.5	15	28.5
: 38 :				-105						15						0			
1 40 1				-104						26						-12			
1 42 1				-121						22.5						-17			
1 44 1				-141						-13.						-16			
1 46 1				-148						-63						-20			
1 48 1	-191			-151			-102			-82.			-32			-8			23.5
1 50 1				-183						-63						-1			
1 52 1				-207						-43						21			
1 54 1				-226						-42.						34			
1 56 1				-252						-47						43			
: 58 :				-279						-62						44			
: 60 :	-216	-251	-283	-289	-260	-199	-135	-112	-94.	-85	-82	-80	-66	-47	-10	22	34	11	-38
1 62 1				-287						-94						-15			
1 64 1				-282						-90						-44			
1 66 1				-268						-93						-62			
1 88 1				-244						-112						-85			
1 70 1				-225						-136						-107			
1 72 1	-246			-218			-189			-162			-130			-114			-106

DISTORTION OF 1/8" PLATE AFTER PANELS 1 AND 7 WERE HEATED THE THIRD TIME

TRANSVERSE

CONTINUE PROCESS. SAMESS STREETS ACCOUNT SERVING SAMESSES

										1 (CHIX)) V L N J L	•								
		0	2	· ·	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
	0	: -132		-	-148			-145			-155			-142			-158			-168
ļ	2				-144						-123						-145			
	4				-162						-96						-124			
	6				-186						-90						-97			
	8	1			-200						-96						-78.			
į	10	!			-205						-91						-71			
;	12	-158	-186	-207	-203	-176	-133	-113	~87	-74	-71	-74	-77	-75	-71	-65	-65	-68	-76	-71
į	14	;			-187						-53						-56.			
1	16	}			-158						-35						-58			
1	18	1			-135						-13.						-59			
1	20	;			-130						-7.5						-47			
į	22	;			-131						-32						-26			
	24	-175			-138			-10C			-68			-38			-14			10
	26	1			-163						-51						-17			
	28				-175						-34						-10			
	30	!			-169						-35						-4			
	32				-155						-36						-7			
	34				-139						-20						-6			
		-172	-160	-143	-123	-106	-96	-90	-46	-12	0	-6	-21	-26	-15.	-4	1.5	6	12	25.5
	38	1			-107						15						-2.5			
i	40	:			-105						25						-14			
	42				-121						21						-19			
1	44	:			-139						-16						-19			
1	46	1			-146						-65						-22			
	48	-191			-152			-104			-84			-33			-10.			20.5
	50				-166						-62.						-3.5			
	52				-176						-42						17			
	54				-187						-42						31			
	56				-213						-48.						40			
	58				-247						-66		••				41	٠.		
		-212	-238	-264			-187	-136	-115	-99		-85	-82	-68	-49	-12	19	31	7.5	-43
	62				-273						-98						-17			
	64				-271						-91						-46			
	66				-257						-92						-65			
	68				-232						-111						-87.			
	70				-214			4.5.			-135			400			-110			
į	72	-236			-212			-186			-161			-129			-117			-113

DISTORTION OF 1/8" PLATE AFTER PANEL 7 WAS HEATED THE FOURTH TIME

TRANSVERSE

	0	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
0 2 4 6 8 10 12 14 16																			
: 20 : 22 : 24 : 26 : 26 : 28 : 0 : 30 : N : 32 :	-175			-139 -164 -176 -170 -156			-101			-69 -52. -34 -35 -35			-39.						
G: 34: I: 36: T: 38: U: 40: D: 42: E: 44:	-172	-160	-142	-139 -123 -106 -104 -120 -138 -146		-96	-91	-48		-19 0 14 24 19 -17 -68	-5.5	-21	-27						
; 46 ; 48 ; 50 ; 52 ; 54 ; 56 ; 58 ;	-191			-154 -155 -159 -165 -186 -219			-105			-85. -62. -42 -41 -49 -66			-35						
: 60 : : 62 : : 64 : : 66 : : 70 : : 72 :		-227	-242			-175	-135 -185	-116			-86	-84	-68 -131						

aptent precedentsbesobbilisectivent zoezeze bedeede helekken prezeze bedeen zoezeze keezeze bedeel K

DISTORTION OF 1/8" PLATE AFTER PANELS 7 AND 1 WERE HEATED THE FOURTH TIME

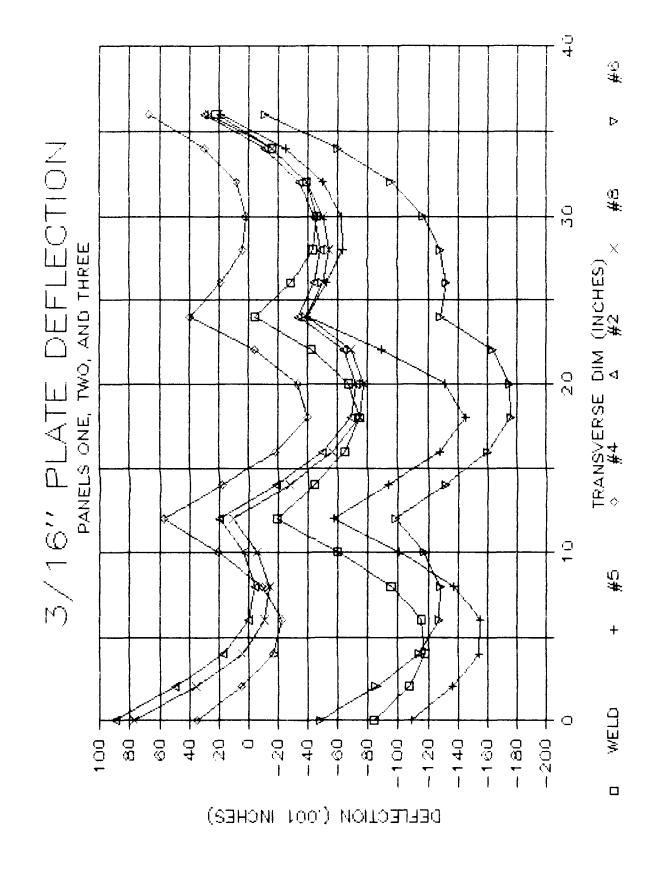
0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 1 0 1 -134	
2 -143	36
: 4 : -155 -99 : 6 : -172 -93 : 8 : -177 -100 : 10 : -173 -96	
: 4 : -155 -99 : 6 : -172 -93 : 8 : -177 -100 : 10 : -173 -96	
8	
: 10 :	
: 10 :	
1 10 1 -147 -170 -174 -144 -144 -110 -114 -00 -77 -74 -75 -70 -70	
(12 (-103 -1/2 -1/4 -104 -114 -110 -110 -170 -7/• -// -/4 -/3 -/0 -/0	
14	
1 16 1 -125 -34	
18 1 -113 -12	
; 20 ; -117 -7	
1 22 1 -125 -33	
: 24 : -180 -142 -103 -69 -40.	
1 26 1 -166 -54	
L ; 28 ; -177 -37	
0 ; 30 ; -171 -37	
N : 32 : -156 -36	
G 34 -140 -19	
I : 36 : -176 -164 -146 -125 -107 -97 -9147 -12 0 -6 -21 -27.	
T 38 -109 15	
U : 40 : -107 24	
D 42 -123 19	
E 44 -140 -17	
{ 46 } -148 -67	
! 48 ! -194 -155 -105 -85 -34	
† 50 †	
1 52 1	
1 54 1	
1 56 1	
† 58 †	
: 60 :	
ł 62 ł	
1 64 1	
: 66 :	
: 68 :	
ł 70 ł	
; 72 ;	

APPENDIX H

GRAPHS OF THE 3/16" STIFFENED PLATE MID-PANEL DEFLECTIONS AFTER THE FIRST LINE HEATING PASS

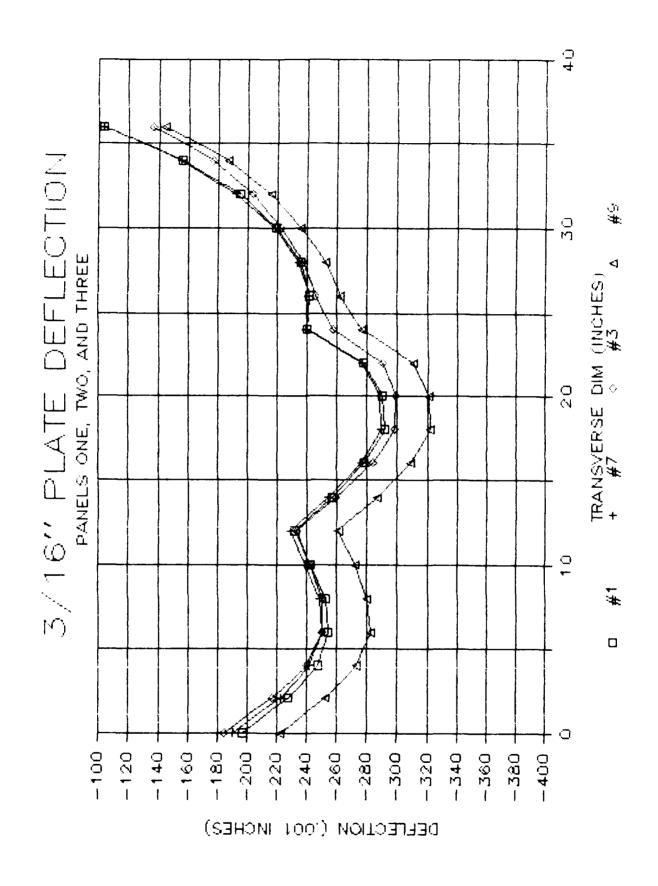
The horizontal coordinate is transverse or longitudinal displacement. measured in inches. and the vertical coordinate is out-of-plane deflection. measured in thousandths of an inch.

OCCOL TOCCOCO MESSESSESSES SESSESSES FOR COCCOCO SECOCOCO SECOCOCO SECOCOCO COCCOCO SESSESSES FESSES S

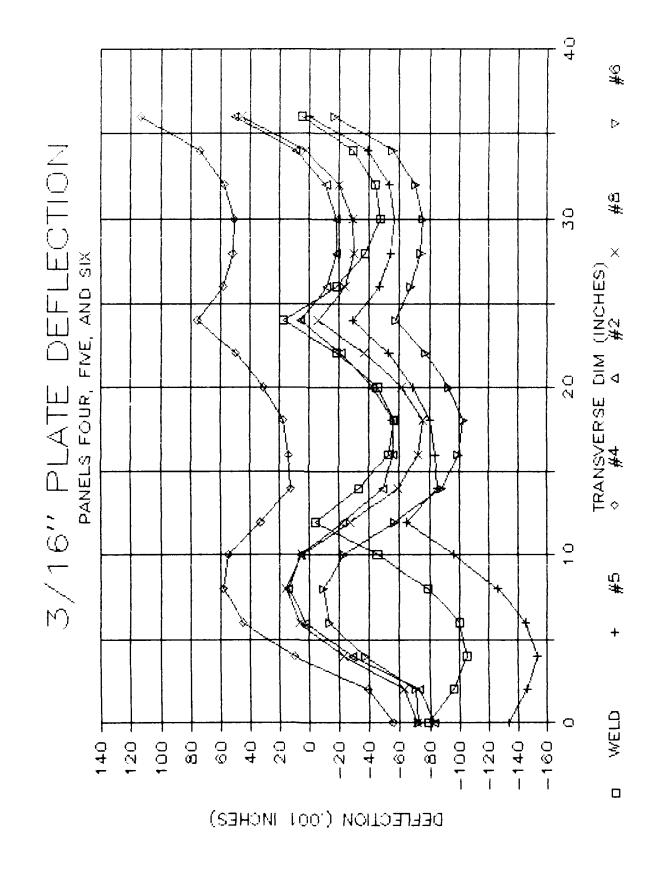


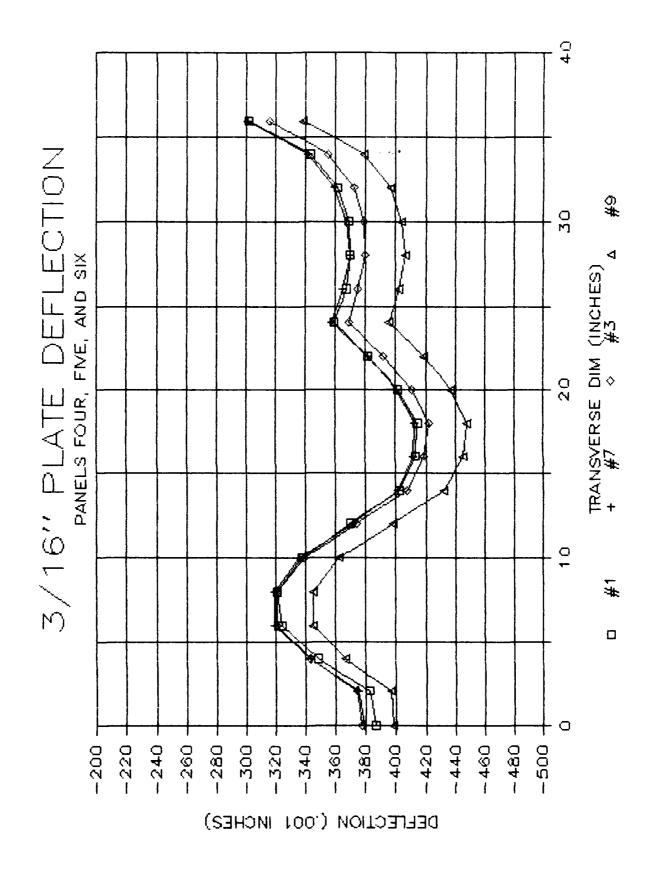
2-2-2-21 10-2-2-2-2-2-2

POSTOCOCO SUSSESSO CARROLL CONTRACTOR CONTRA

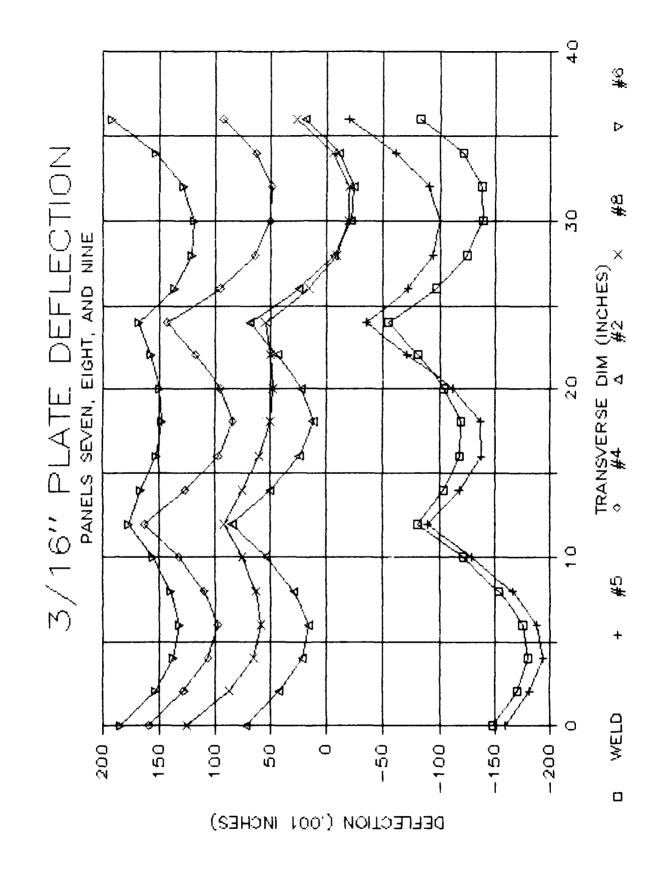


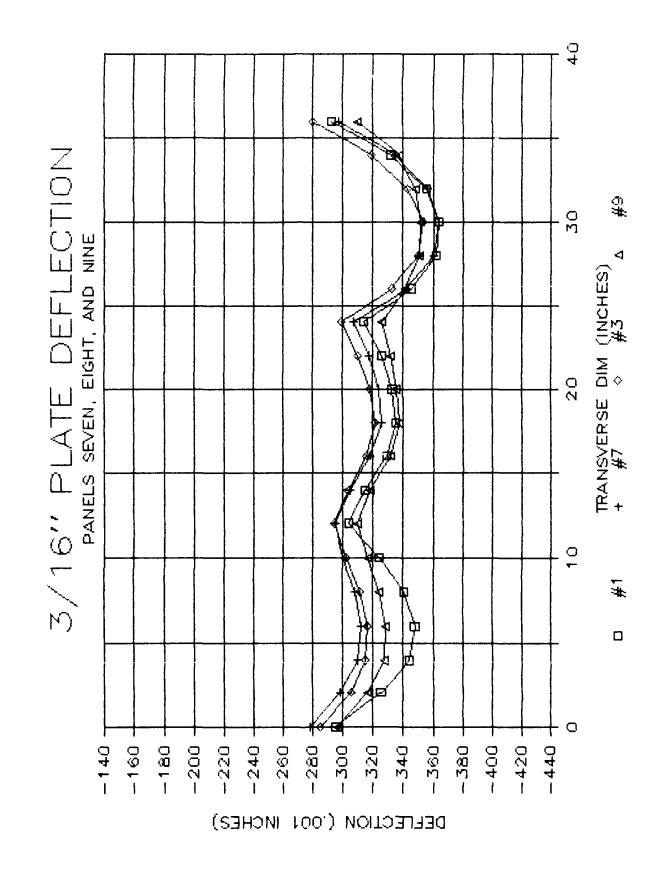
PARAMETER CONTRACTOR INVESTIGATION INTRICTOR INCOMES CONTRACT CONTRACT CONTRACT CONTRACT CONTRACT

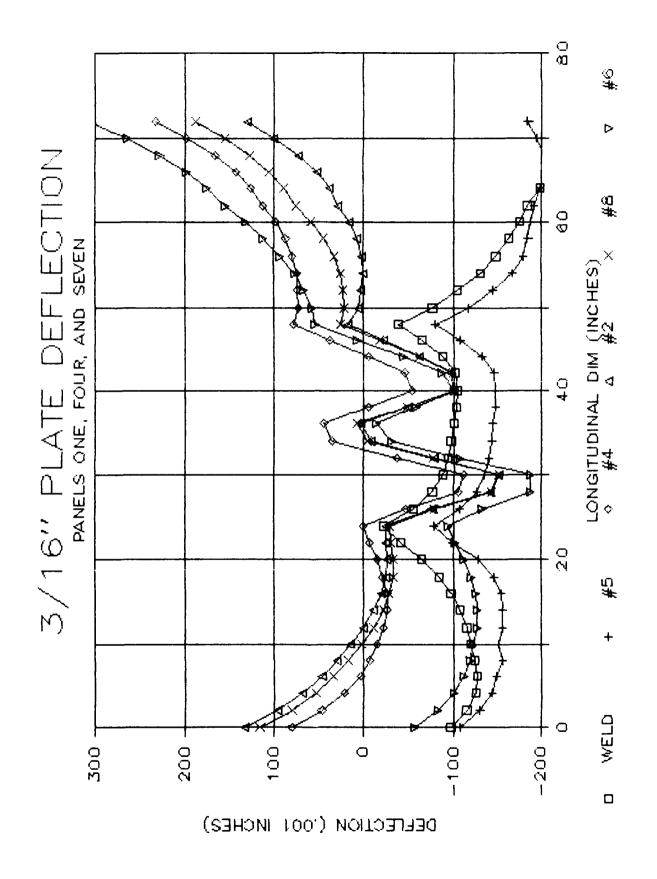




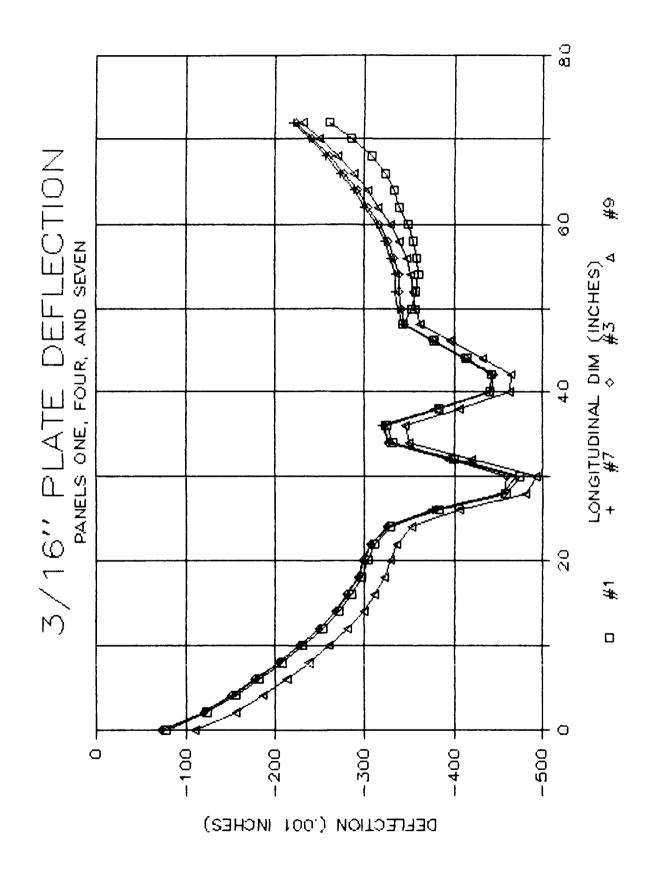
eseral measured increased becaused narrown esercism increased increased increased



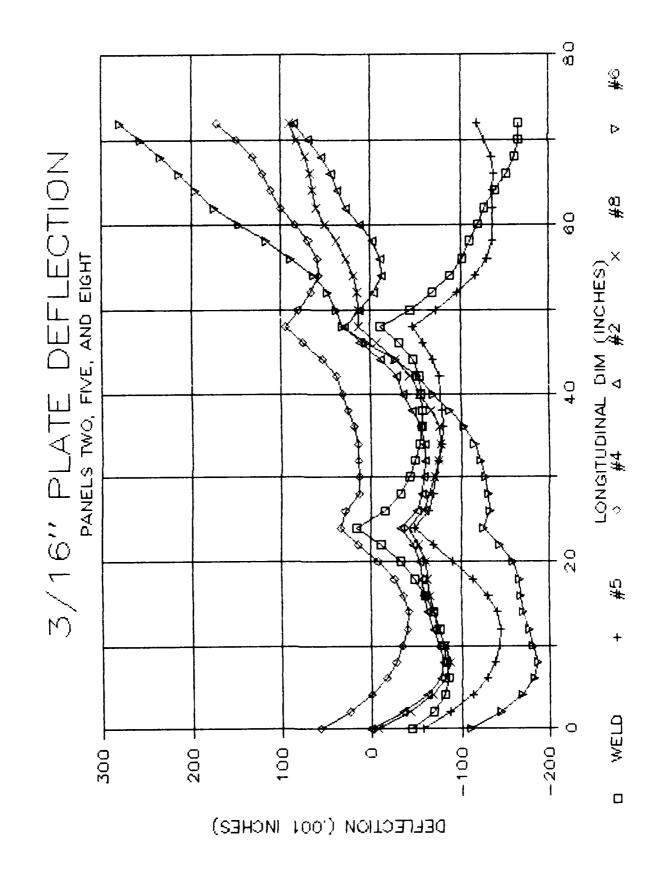




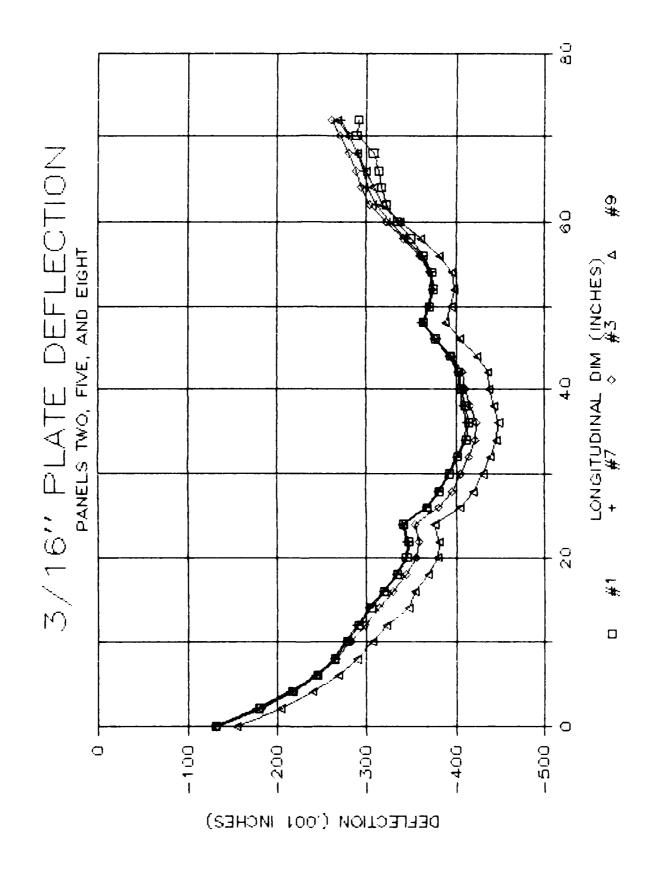
DESERTABLE DESCRIPTION DESCRIPTION OF SEPERABLE MASSICA ASSOCIATION PROFESSIONALE DESCRIPTION DE MASSICATION DESCRIPTION DE SERVICA DE SERVICA



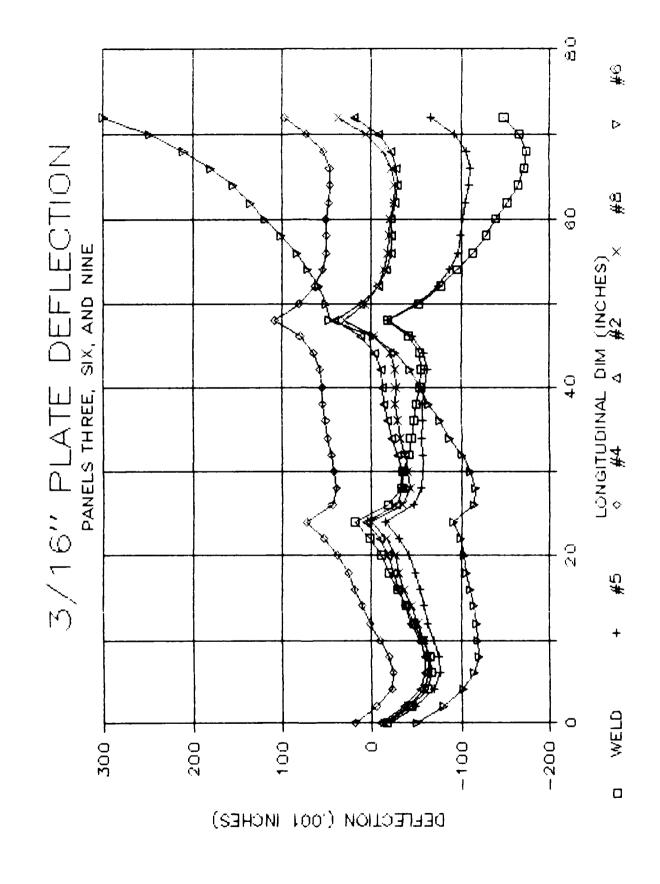
JOSO POD DESTABIO ASSESSO DEFENDA CON TOS OPERAR OPPRINTED PRESERVA CONTRACTOR DE CONT

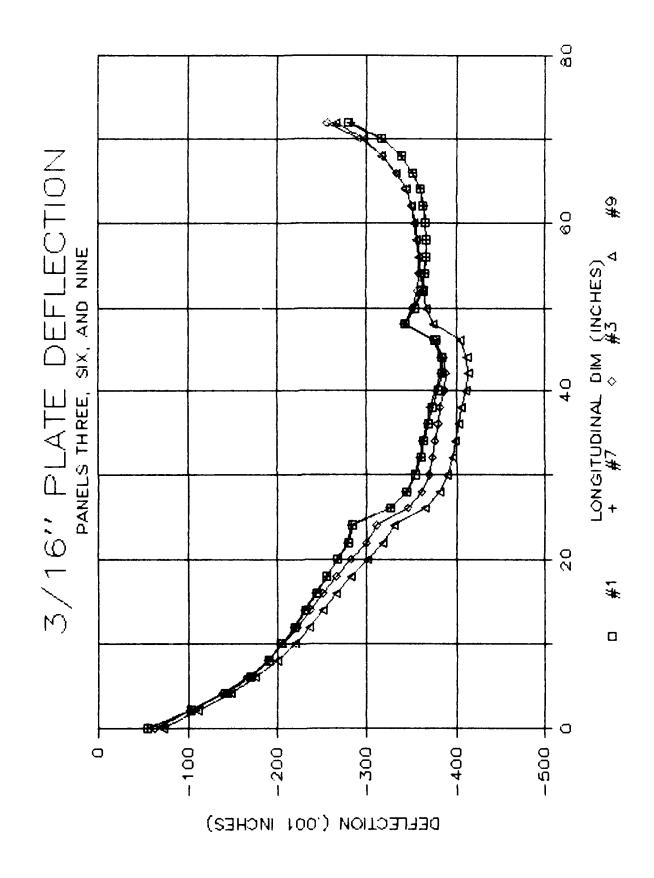


数数对了这样的人们可能够够多数,是是我的话,我的的现在,我的的意思,这句句的说,*是是自己的。在他的时候,我还是是是一个是是*的。 第



CONTRACTOR OF THE PROPERTY OF



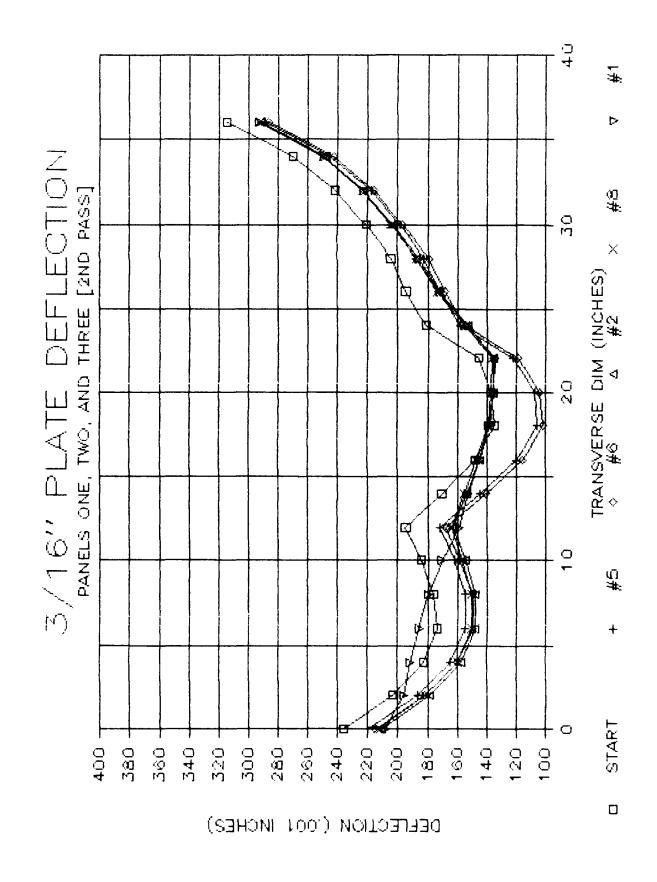


APPENDIX I

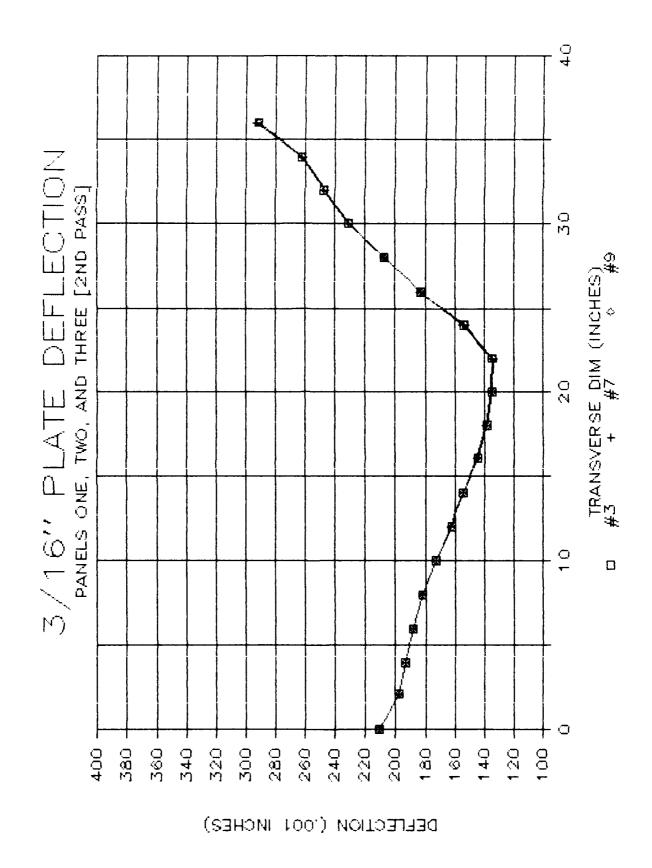
GRAPHS OF THE 3/16" STIFFENED PLATE MID-PANEL DEFLECTIONS AFTER THE SECOND LINE HEATING PASS

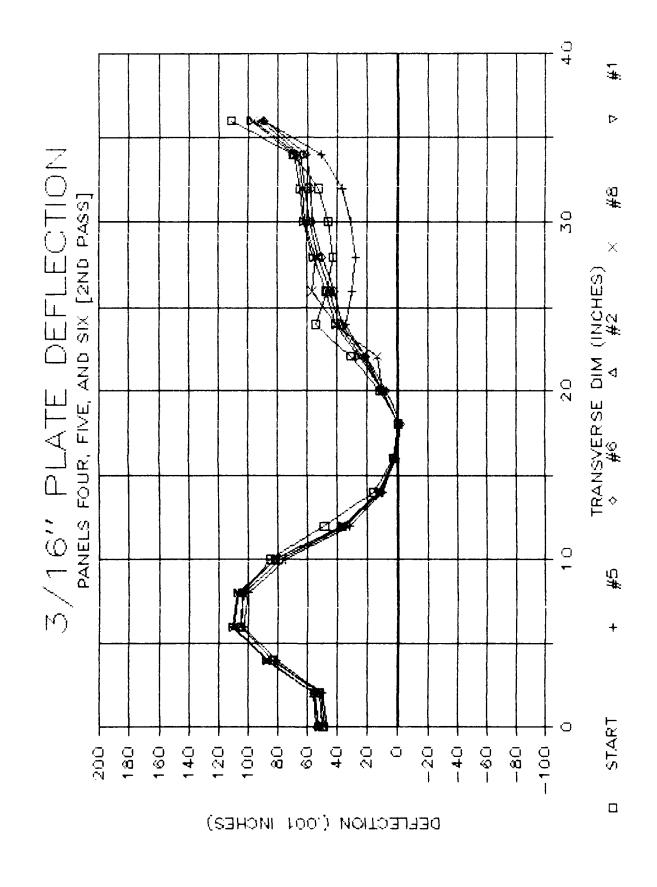
The horizontal coordinate is transverse or longitudinal displacement, measured in inches, and the vertical coordinate is out-of-plane deflection, measured in thousandths of an inch.

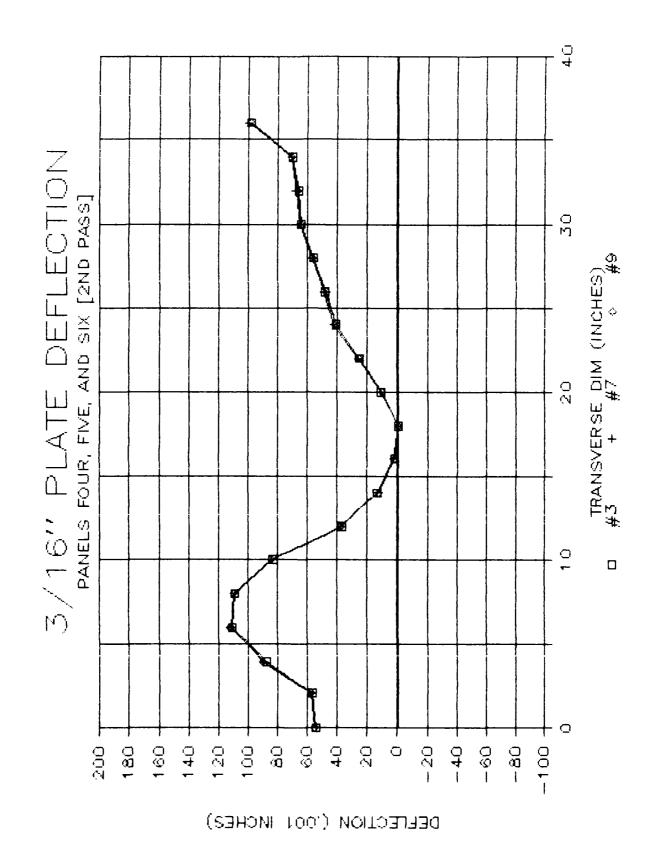
STATE ASSOCIATIONS OF SECURIOR FOR SECURIOR PROPERTY SECURIOR SECURIOR SECURIOR SECURIOR SECURIOR SECURIOR PROPERTY SECURIOR SE SECURIOR S



BECOMES ASSESSED AND DESCRIPTION OF PROPERTY OF STREET, SEPARATE AND ASSESSED ASSESSED ASSESSED.

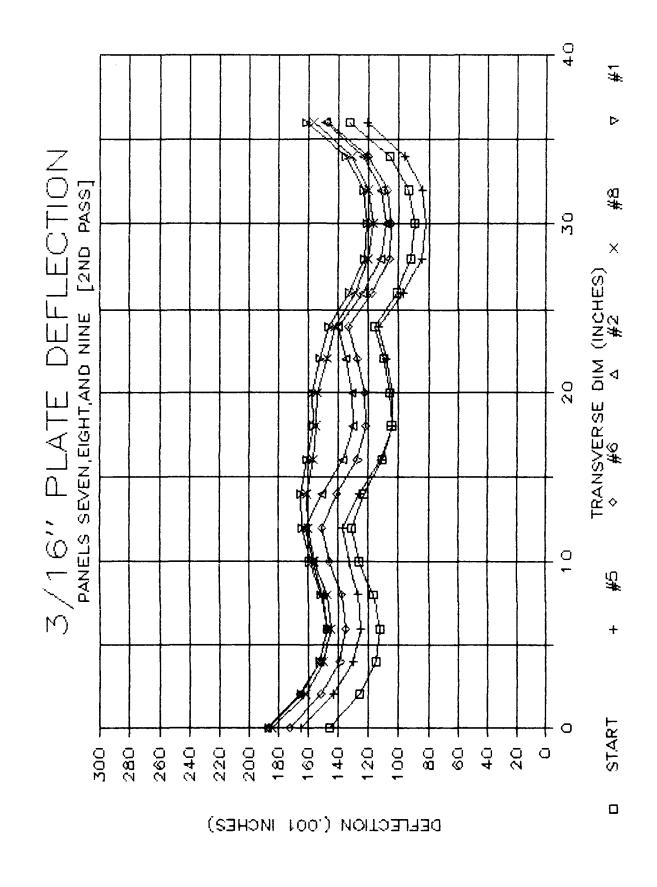




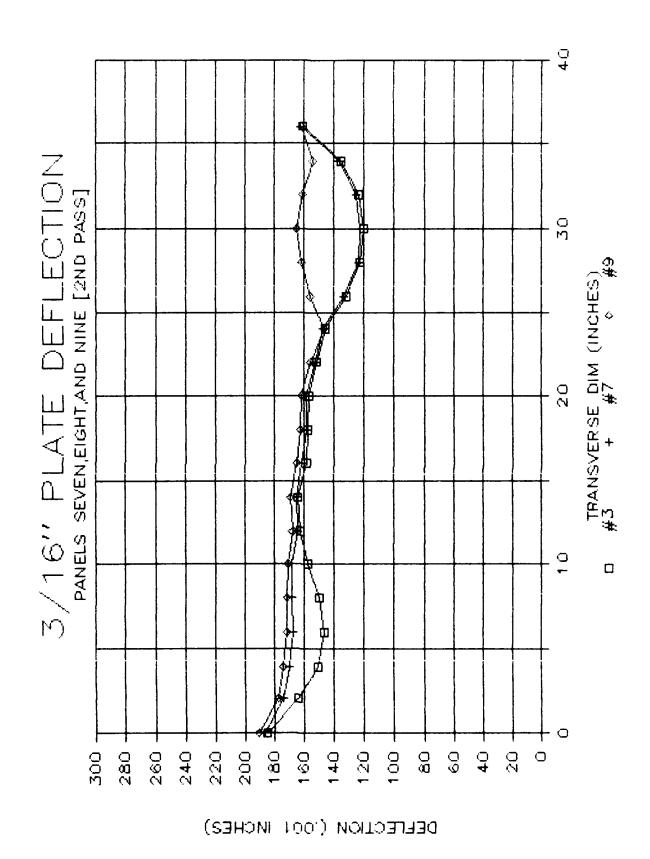


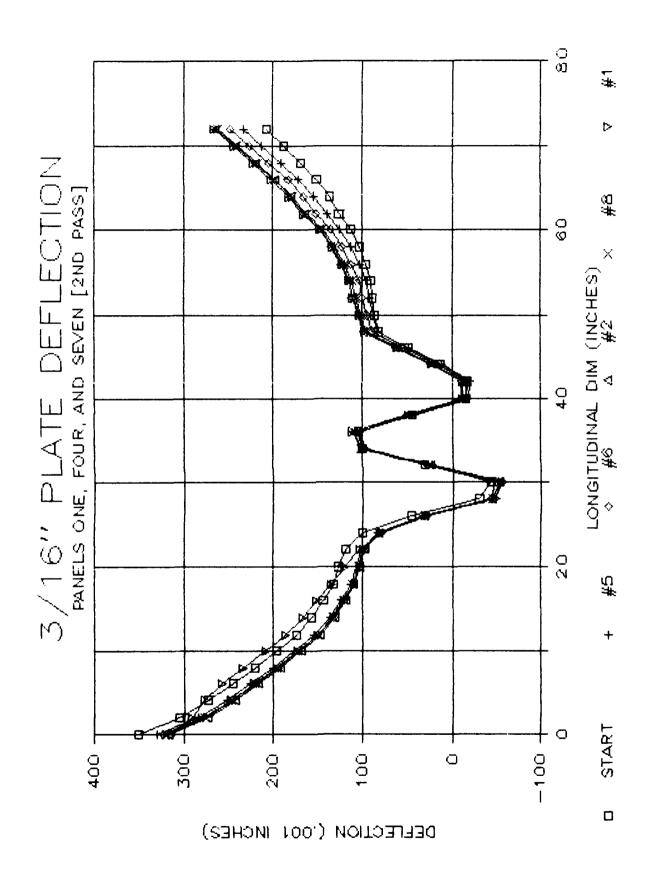
SEES PROPERTY RECEIPED PROPERTY RESERVED BESTER OF

THE RESIDENCE PROPERTY BESCHOOL TO STATE AND THE PROPERTY OF T

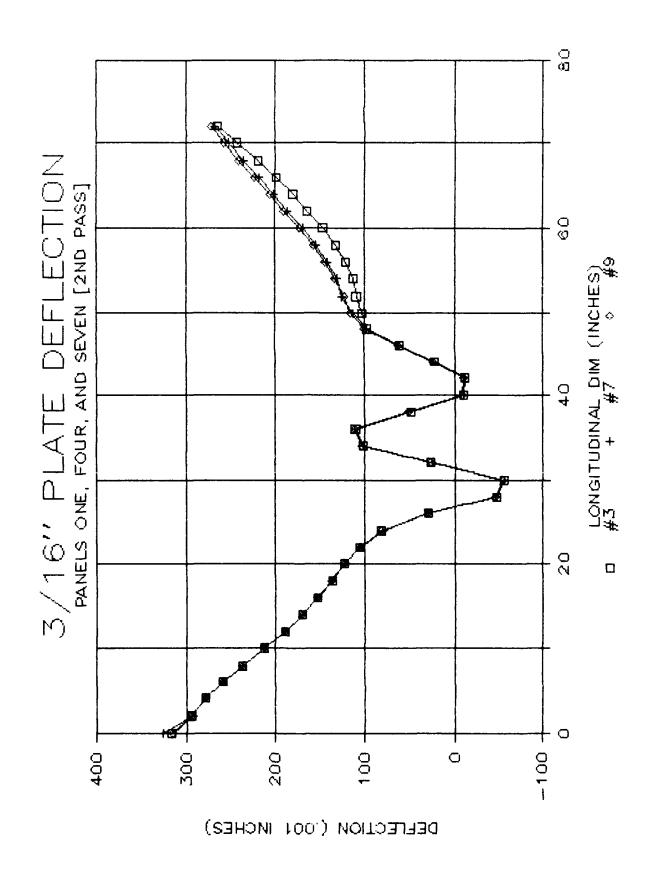


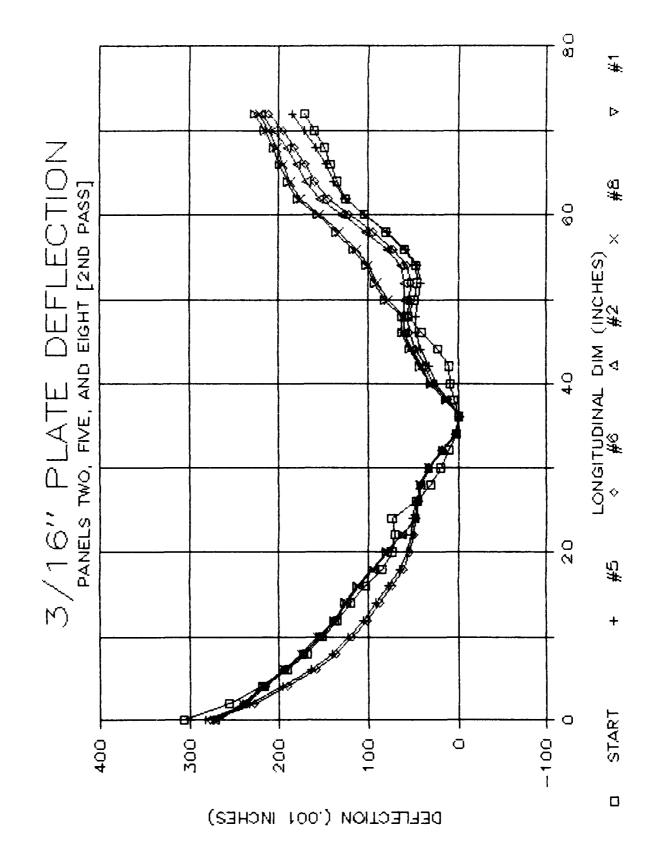
SECOND DESCRIPTION OF THE PROPERTY OF THE PROP

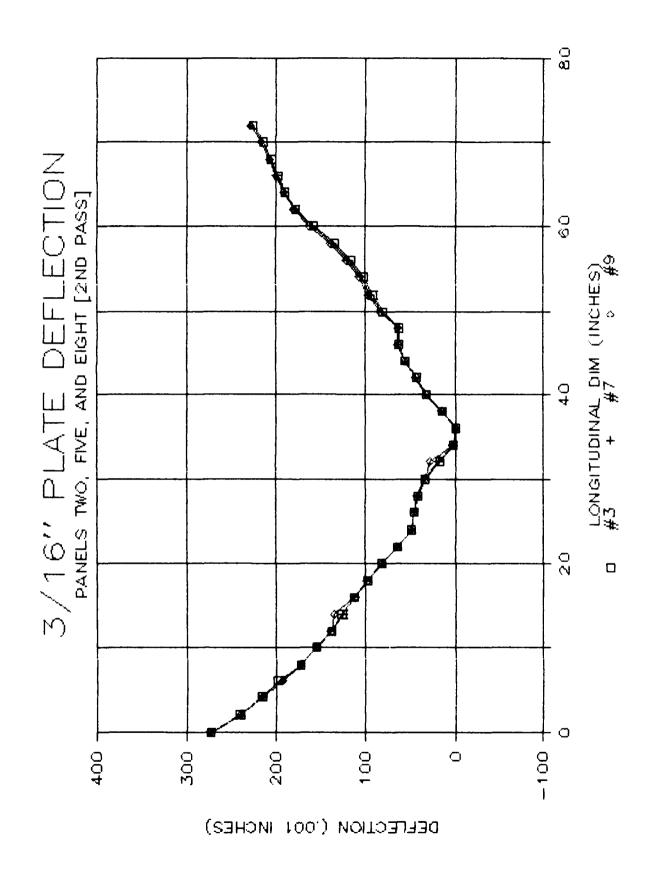


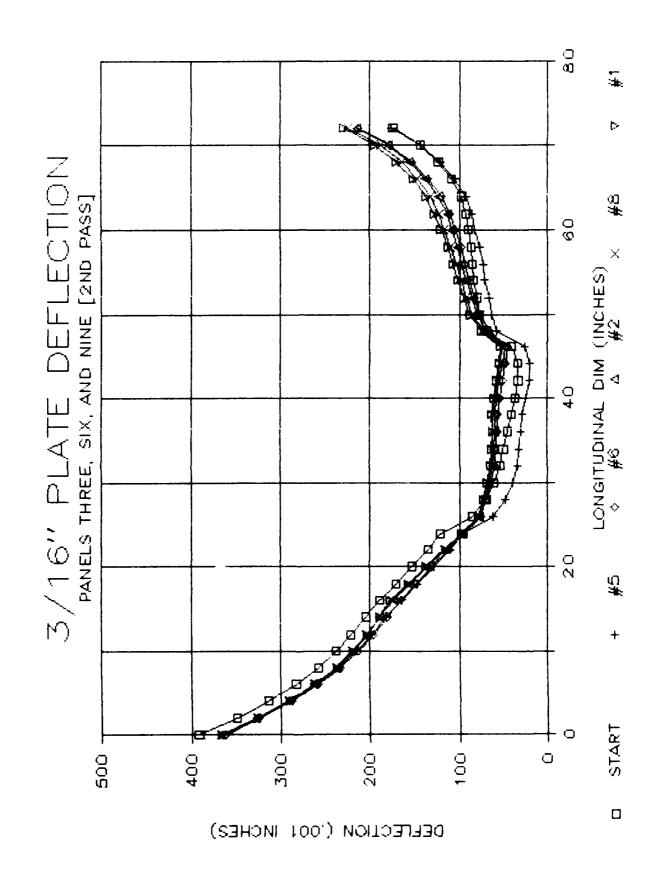


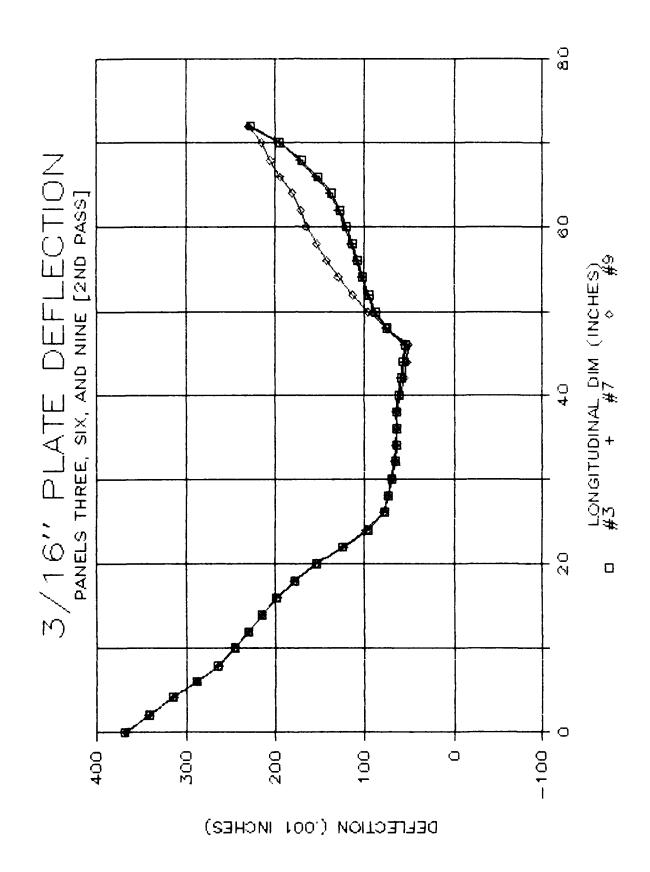
KARIOLO A CAMPONIA POR PROPERTICIO EN PROPERTIMISMO PARTICIONE PAR











THE NEWSCOOL CONTROL STANDS SESSED BESSE

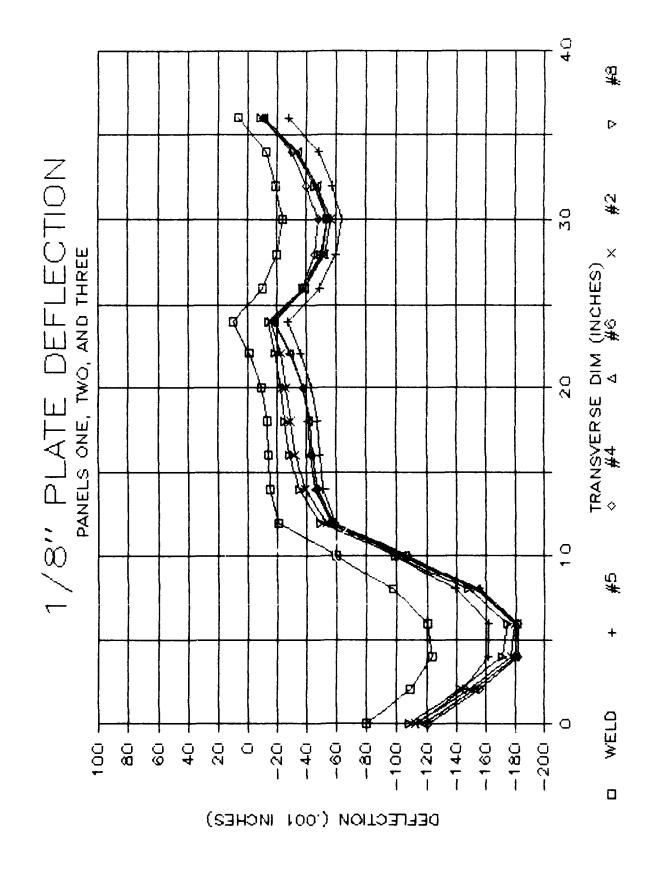
APPENDIX J

GRAPHS OF THE 1/8" STIFFENED PLATE MID-PANEL DEFLECTIONS AFTER THE FIRST LINE HEATING PASS

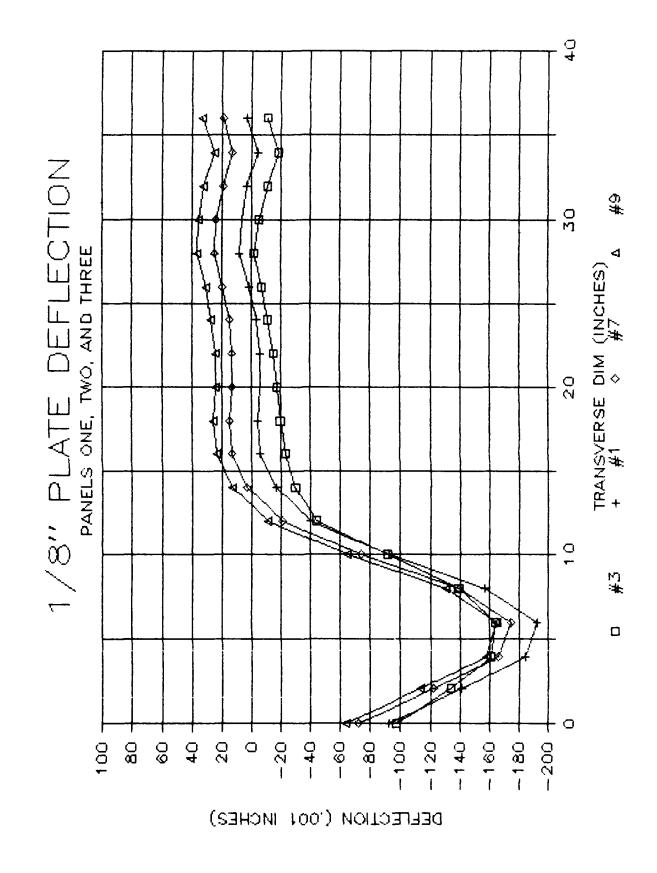
APPEND:

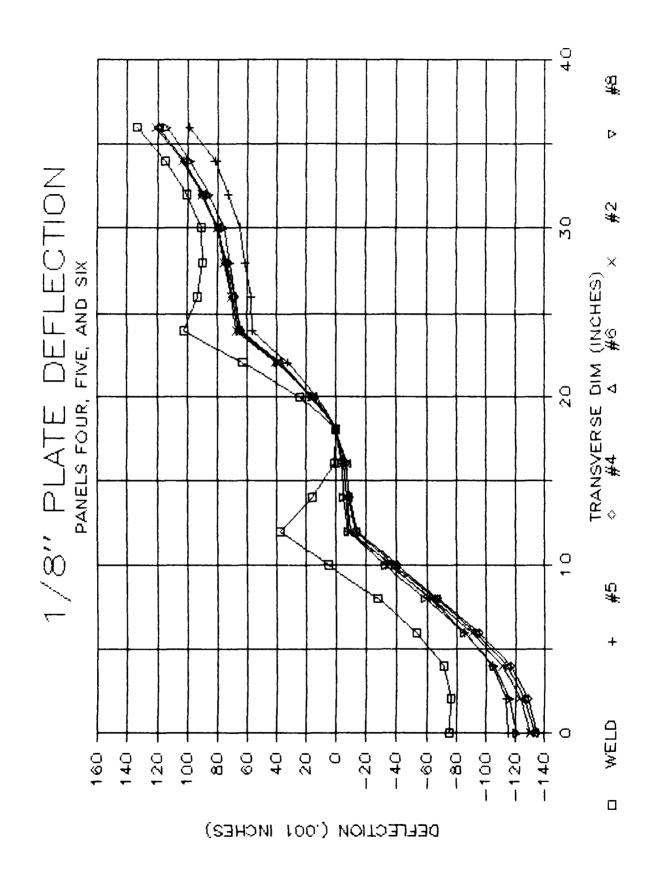
GRAPHS OF THE 1/8" STIFFENED NAFTER THE FIRST LIN

The horizontal coordinate is displacement, measured in inches is out-of-plane deflection, measured. The horizontal coordinate is transverse or longitudinal displacement. measured in inches. and the vertical coordinate is out-of-plane deflection. measured in thousandths of an

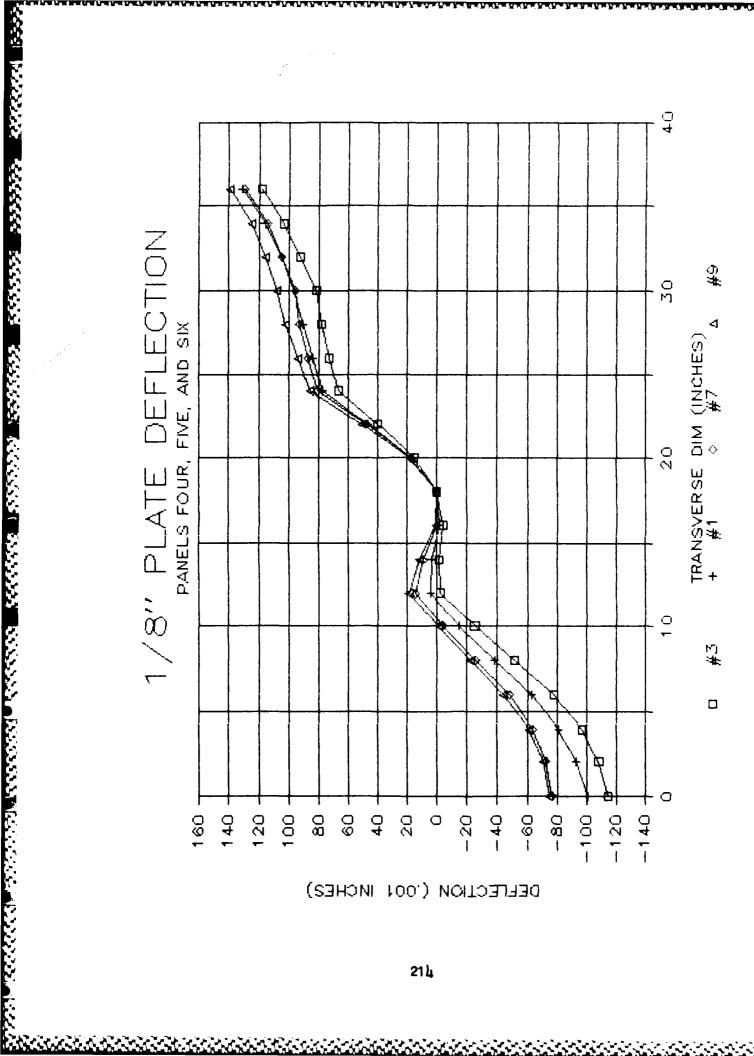


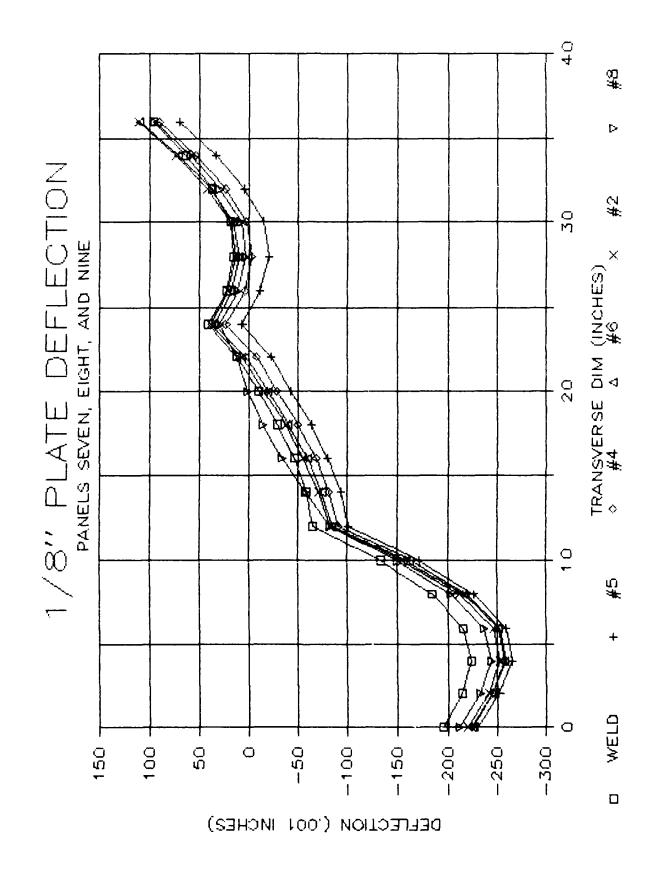
ndesi©eken eerig@keesekusiban ana keesekeegikeesekeesimpeesekeesi maanaan innaan innakeeseki k

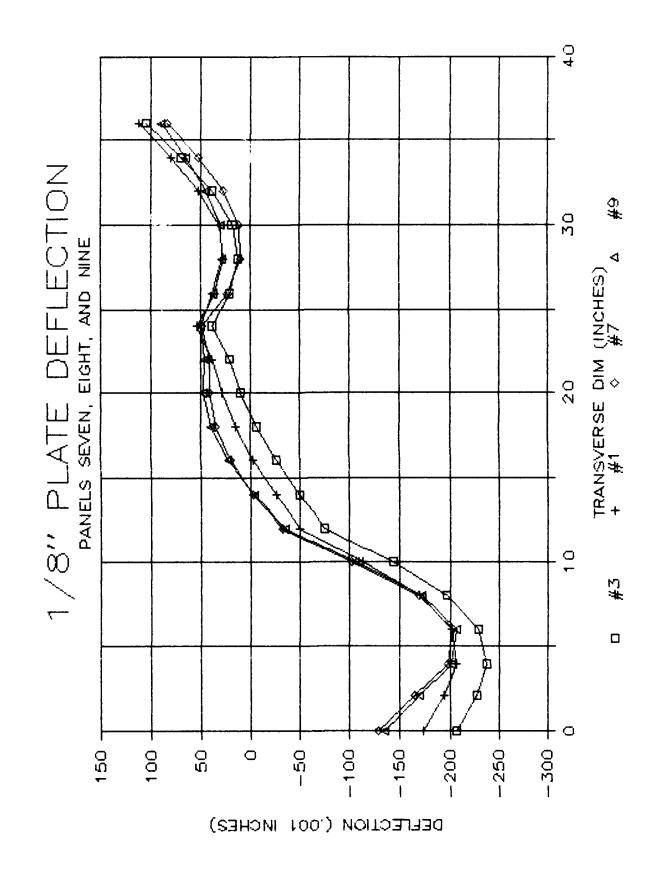


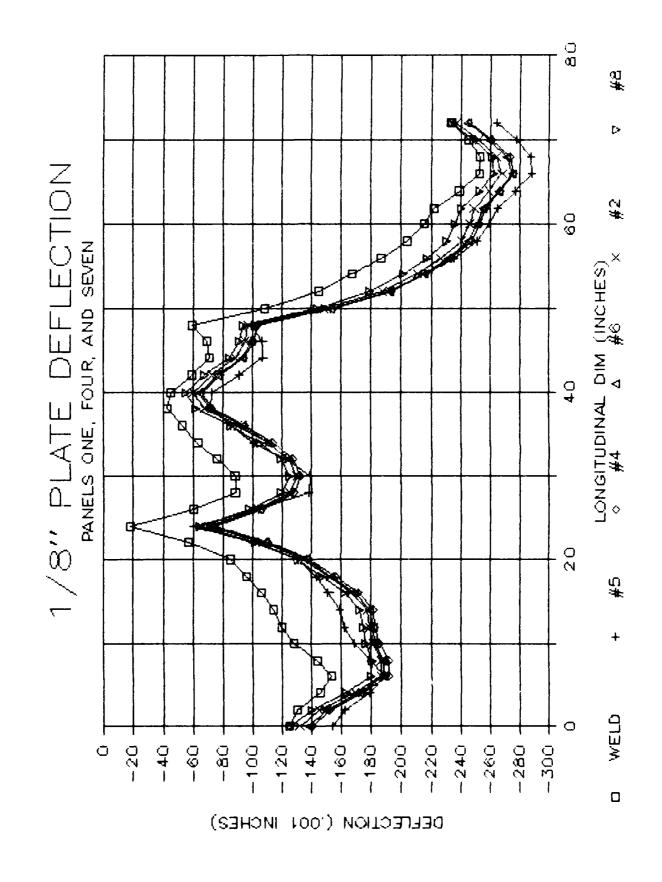


eception accessor ecoesses casses and entry

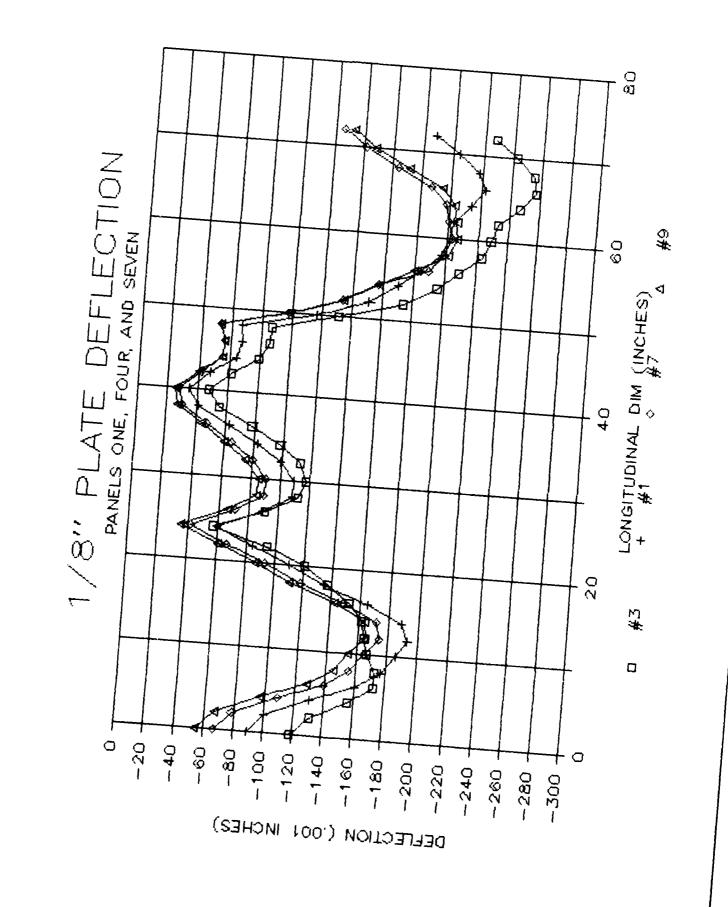




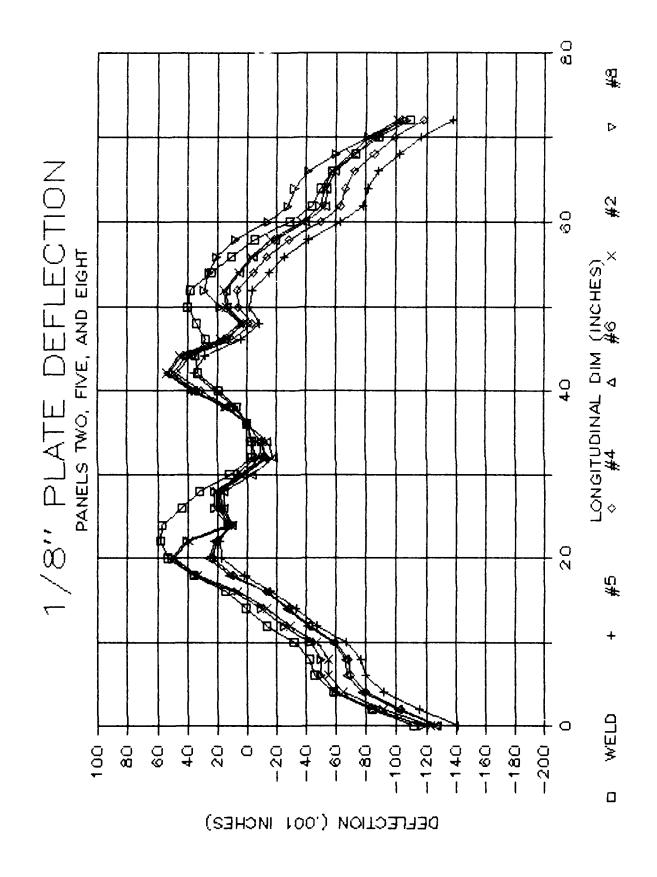




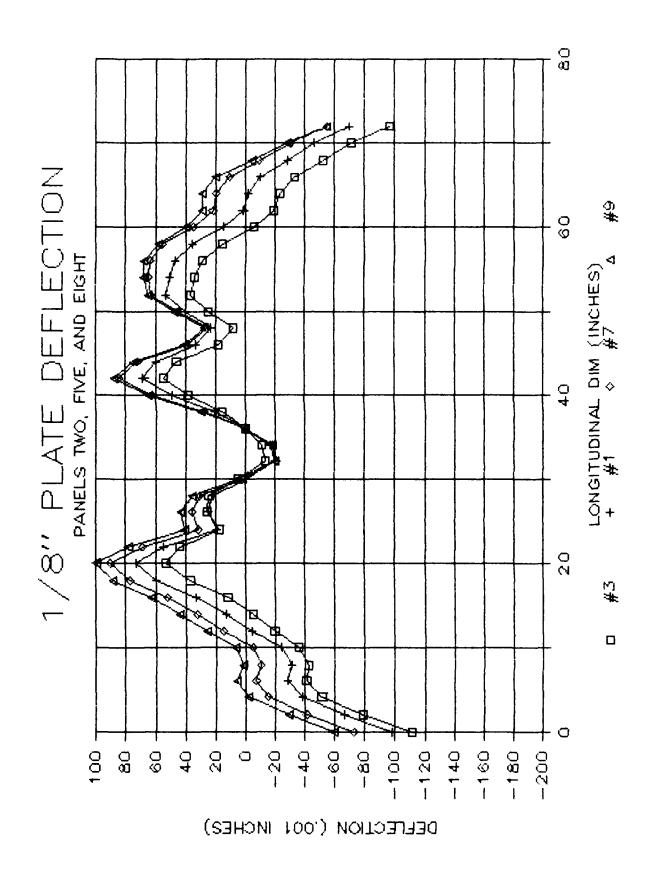
SAM PERCONA PARAMENTAL PROPERTY OF THE PROPERT

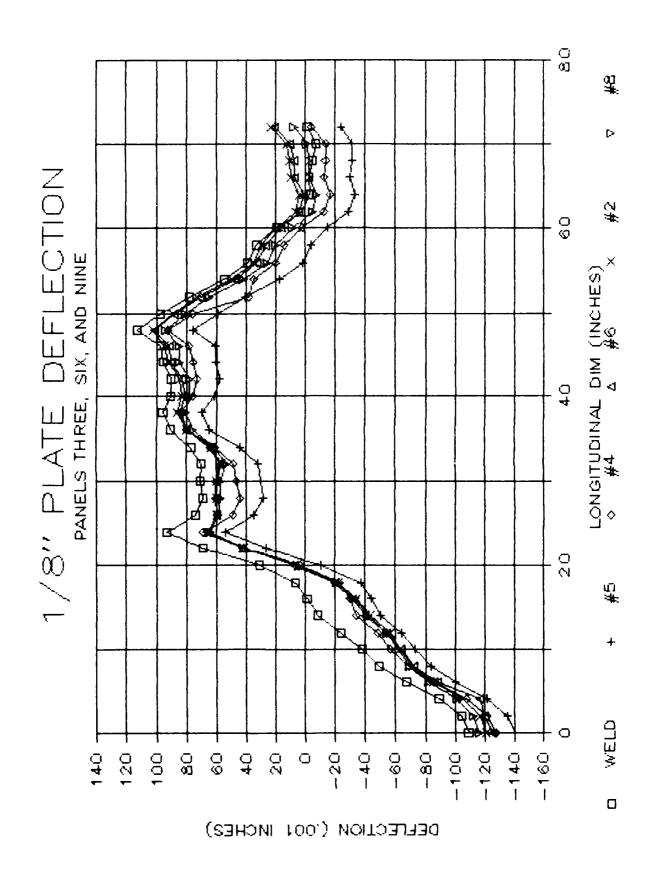


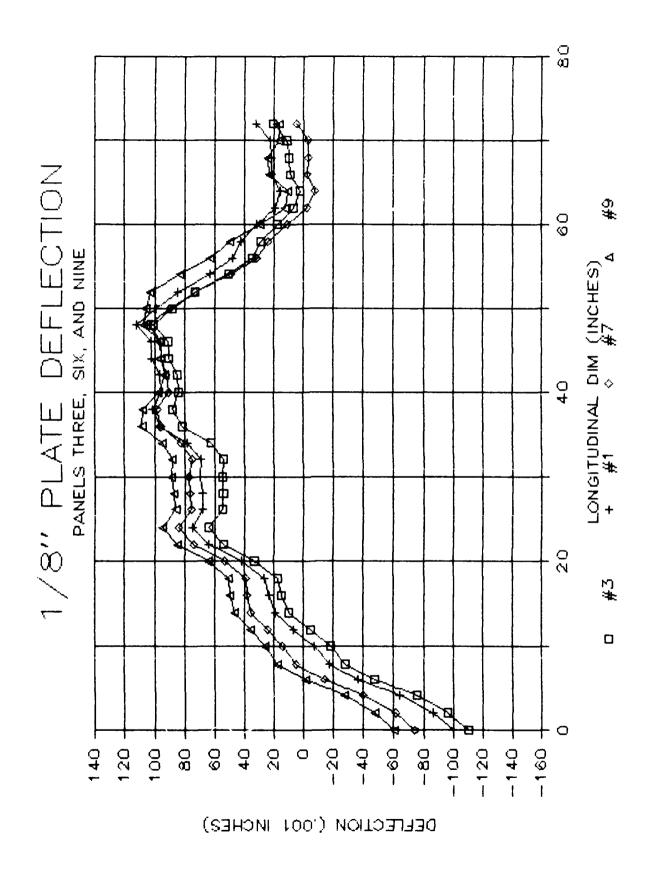
CONTRACTOR NATIONAL BYSINGS (NATIONAL) SOCIETY (NATIONAL) SOCIETY (NATIONAL)



DESCRIPTION OF THE PROPERTY OF





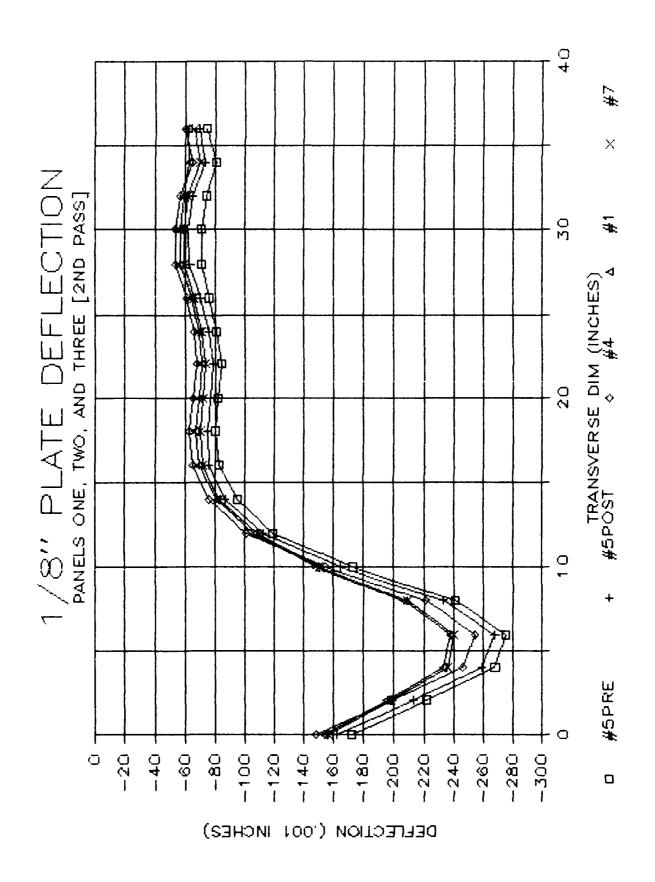


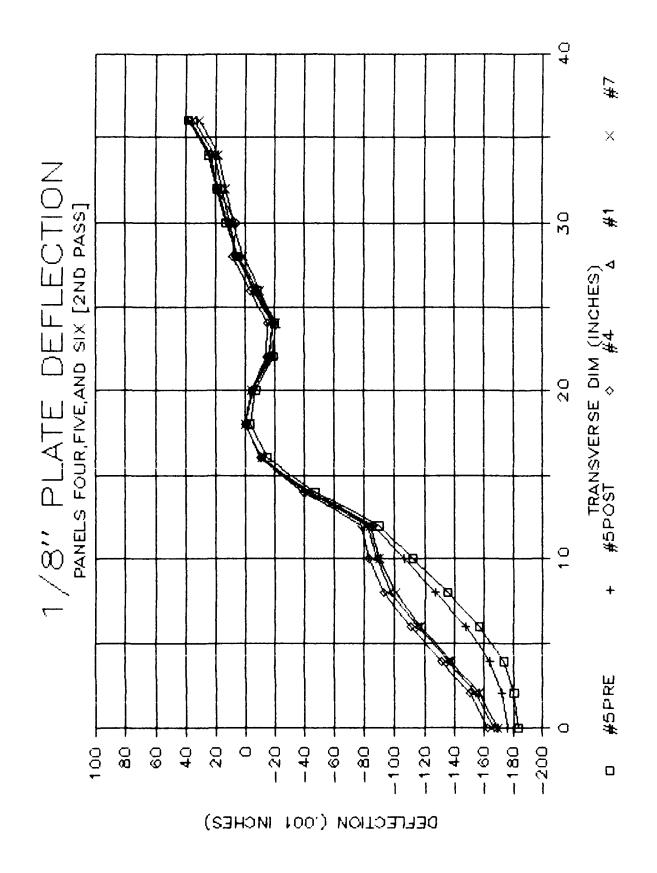
APPENDIX K

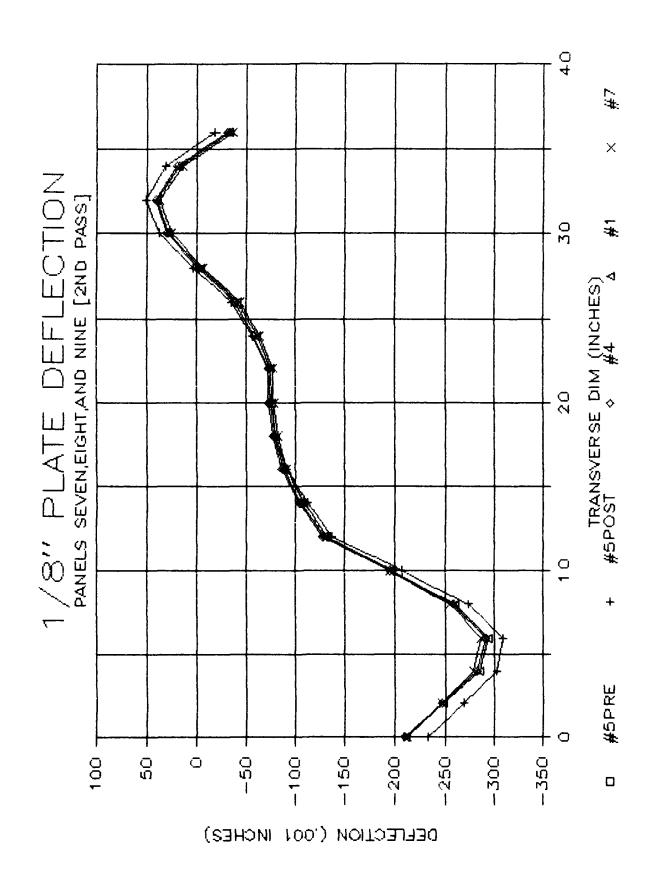
GRAPHS OF THE 1/8" STIFFENED PLATE MID-PANEL DEFLECTIONS AFTER THE SECOND LINE HEATING PASS

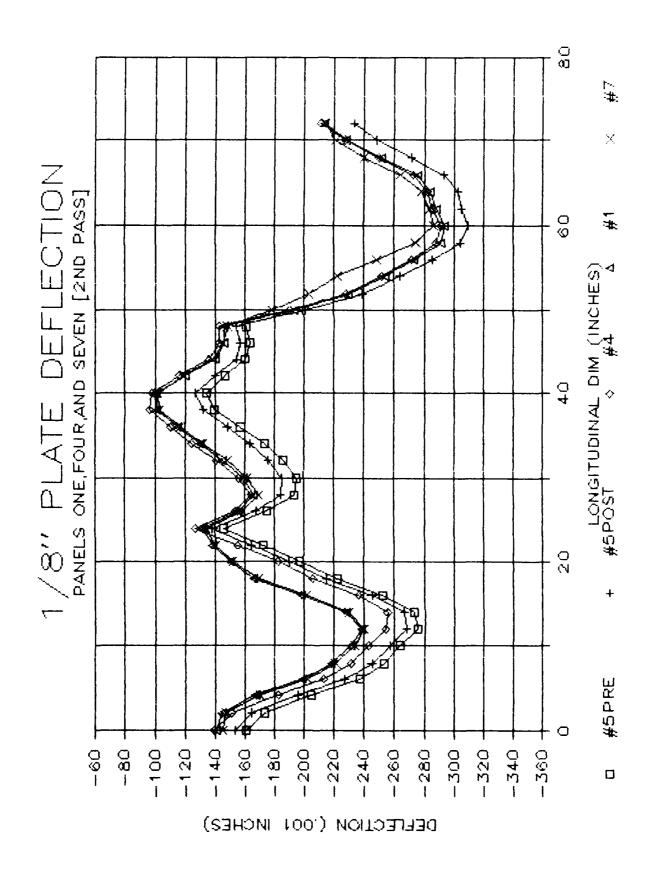
APPEL
GRAPHS OF THE 1/8" STIFFENE
AFTER THE SECOND

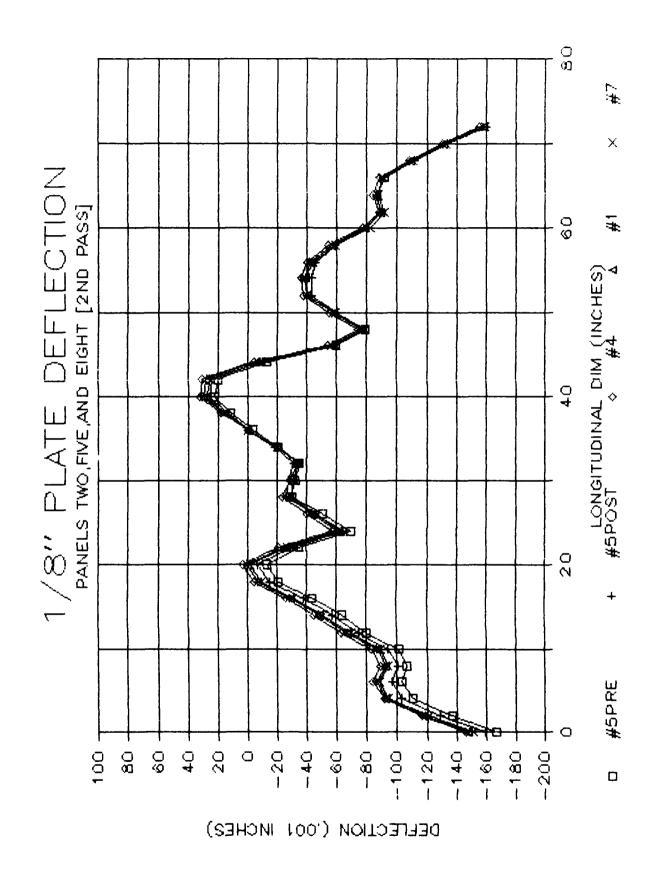
The horizontal coordinate displacement, measured in inchis out-of-plane deflection, mennich. The horizontal coordinate is transverse or longitudinal displacement, measured in inches, and the vertical coordinate is out-of-plane deflection. measured in thousandths of an

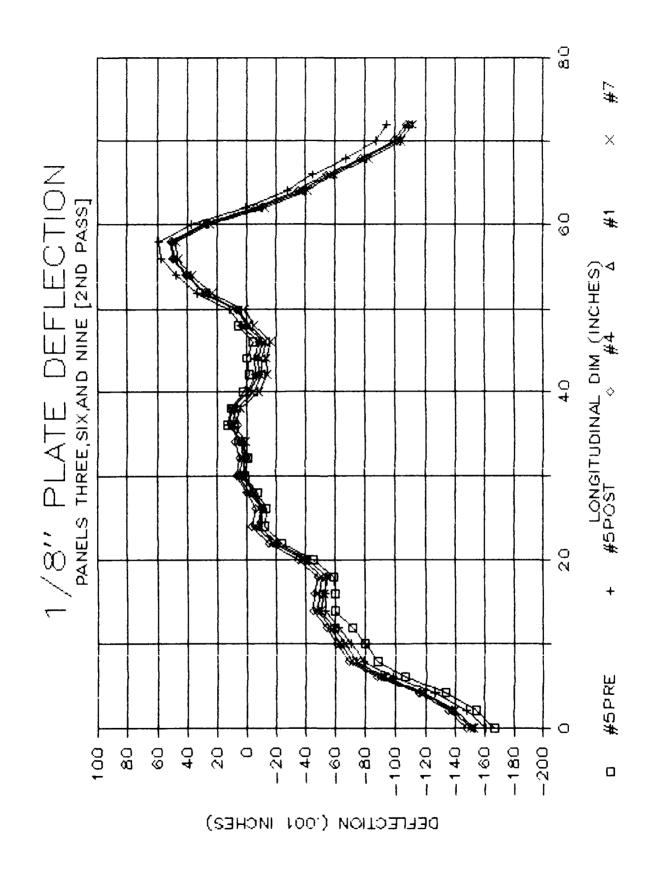












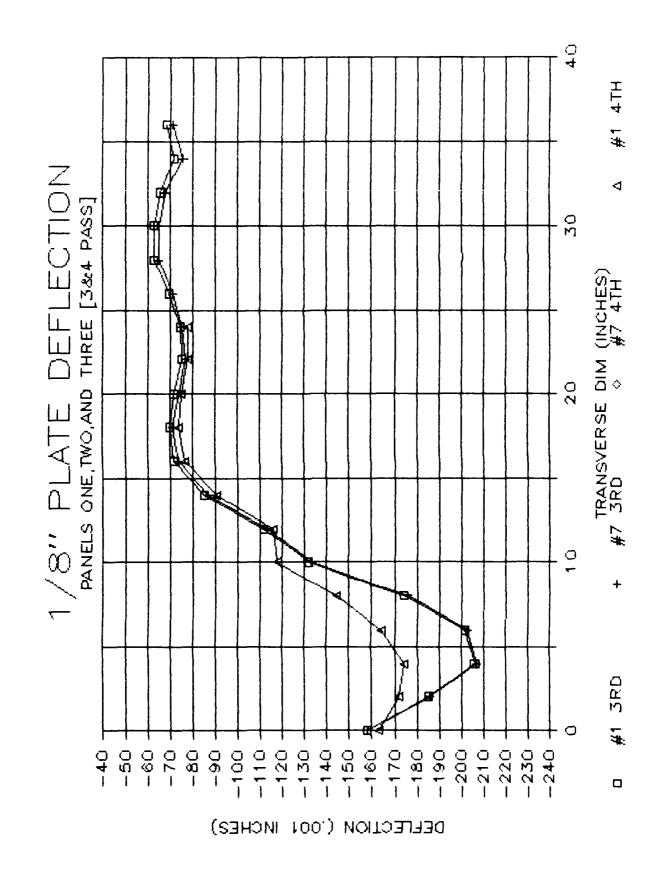
anterestations de la compaction de la comp

APPENDIX L

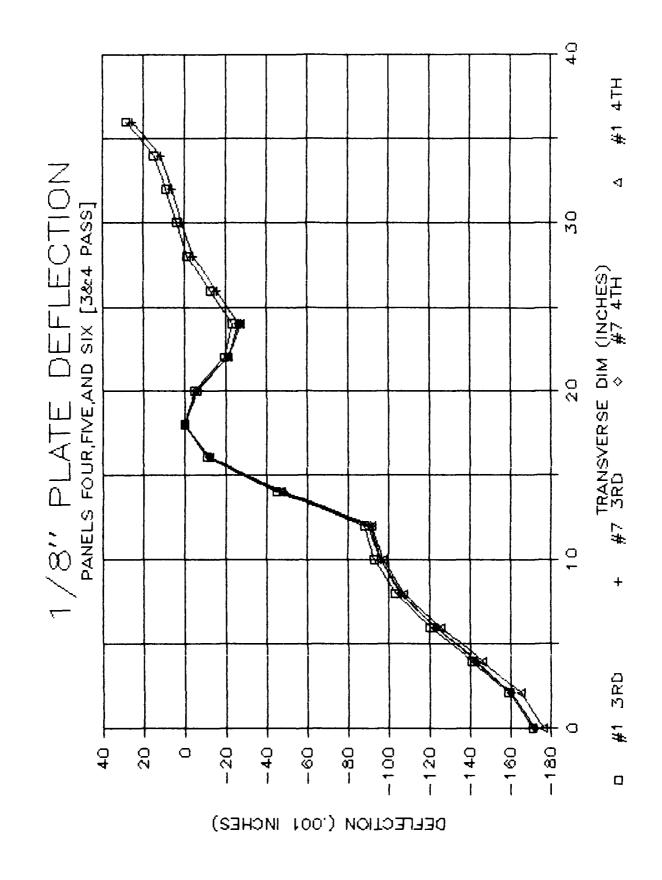
GRAPHS OF THE 1/8" STIFFENED PLATE MID-PANEL DEFLECTIONS AFTER THE THIRD AND FOURTH LINE HEATING PASS

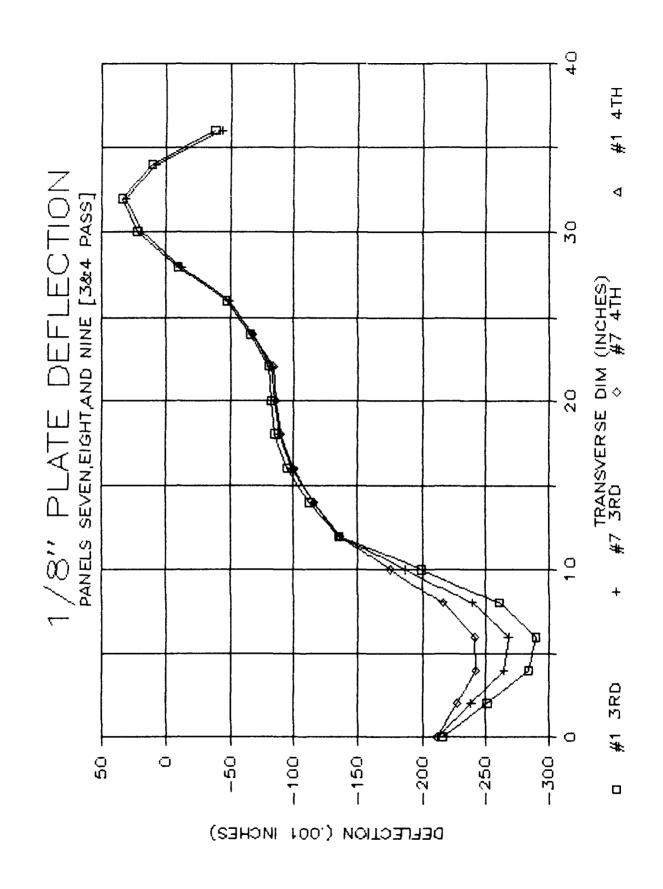
The horizontal coordinate is transverse or longitudinal displacement, measured in inches, and the vertical coordinate is out-of-plane deflection, measured in thousandths of an inch.

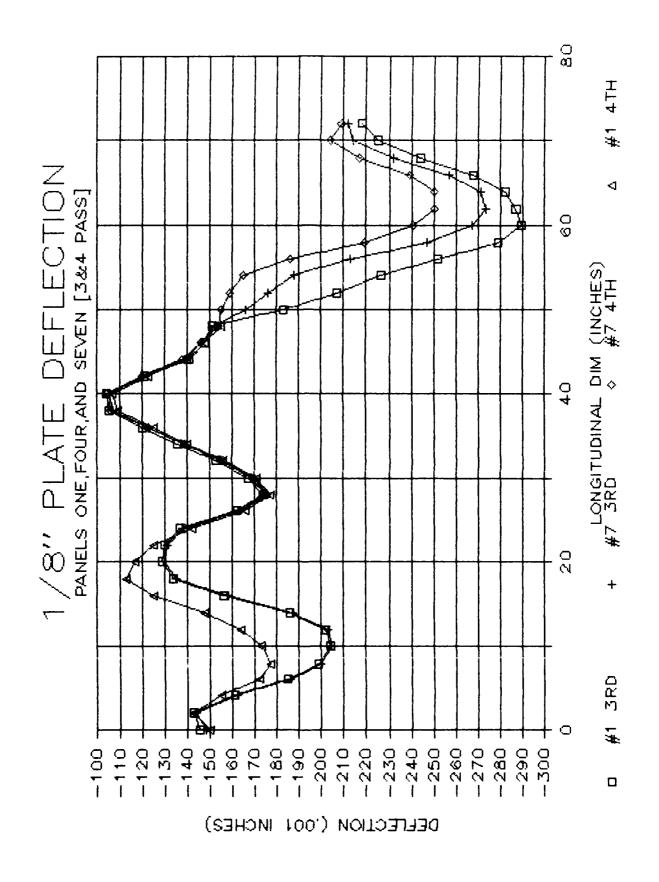
THE PERSON ASSESSED ASSESSED ASSESSED ASSESSED WITHOUT ASSESSED ASSESSED BEARING BEARING FRANCE



K-5X-5X-5X-5X



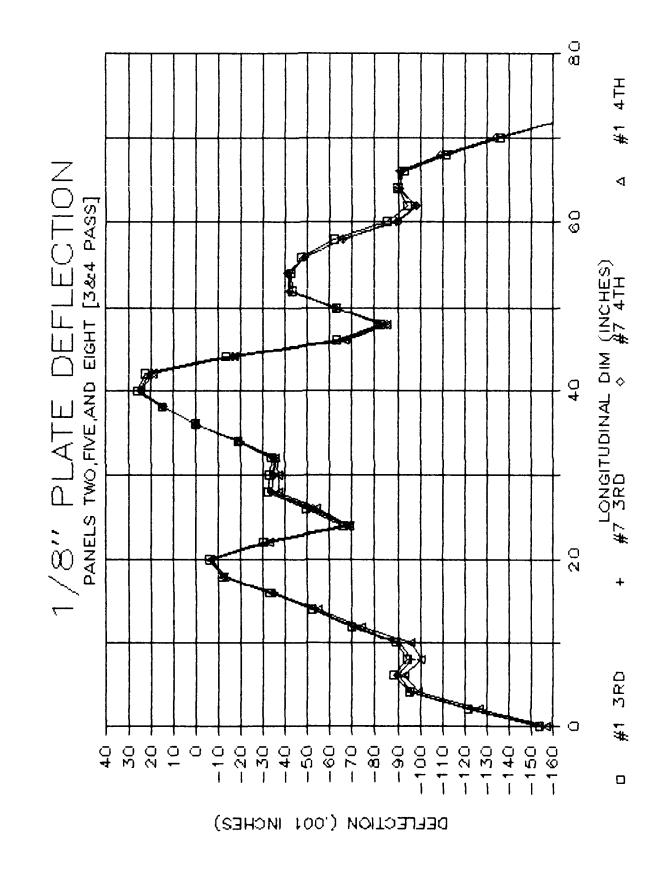


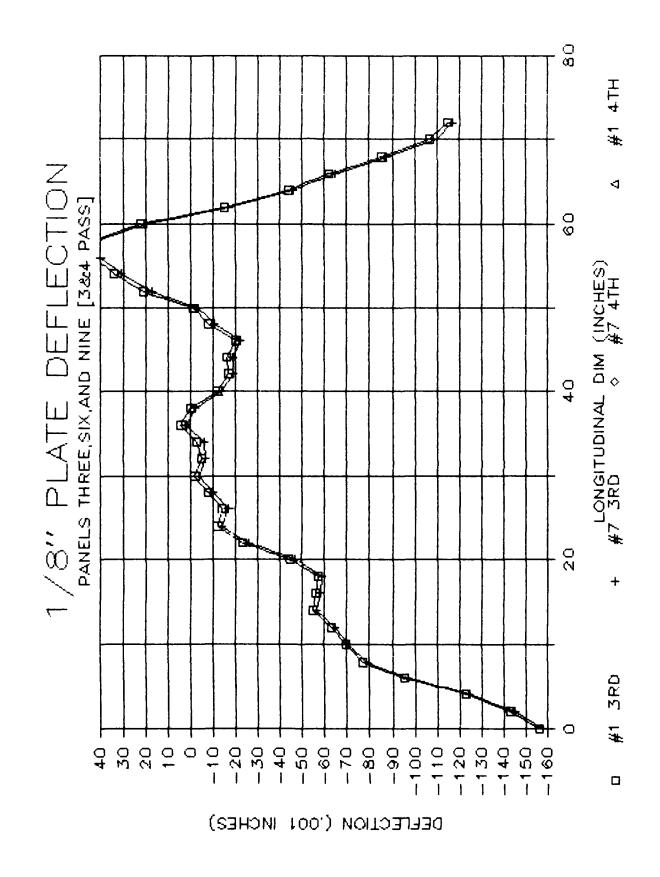


55.6555

CHICAGO CONTRACT

SERVICE OF SERVICES DESCRIPTION OF TAXABLE PROPERTY DESCRIPTIONS OF TAXABLE PROPERTY O





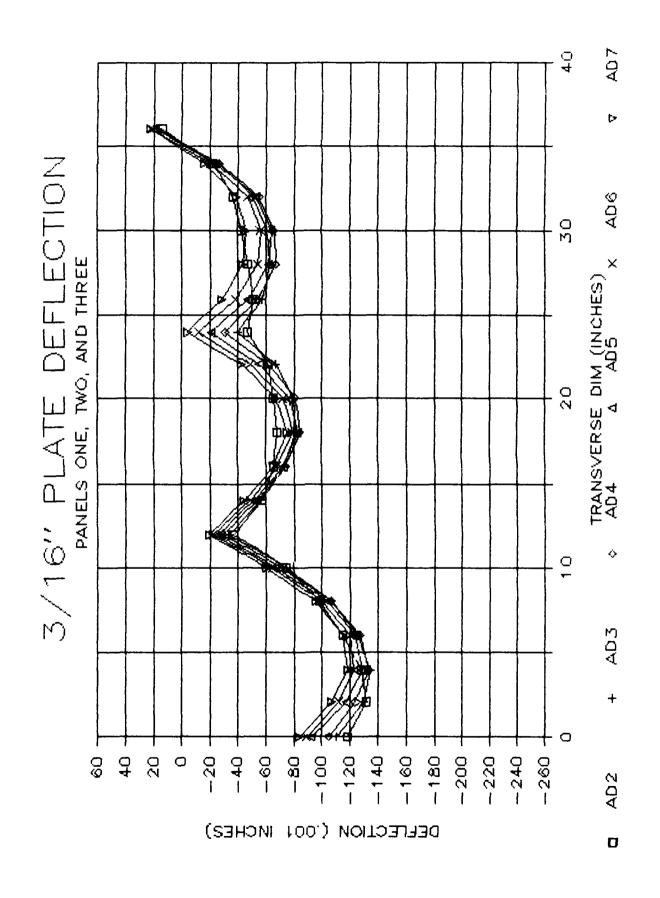
SEER PERFORM CARROLL MASSESS BULLERA GESSELSE COLUMN SANDAN, MISSESS PARFORMASSICAL PRODUCTION

APPENDIX M

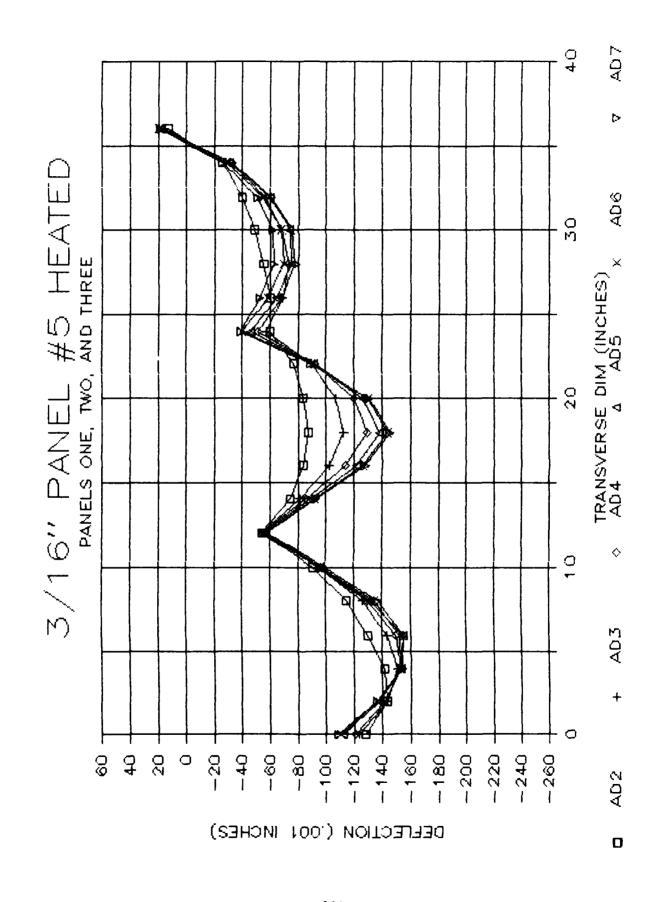
GRAPHS OF THE 3/16" STIFFENED PLATE TRANSVERSE OUT-OF-PLANE DEFLECTION READINGS FOR LINES AD2 THROUGH AD7

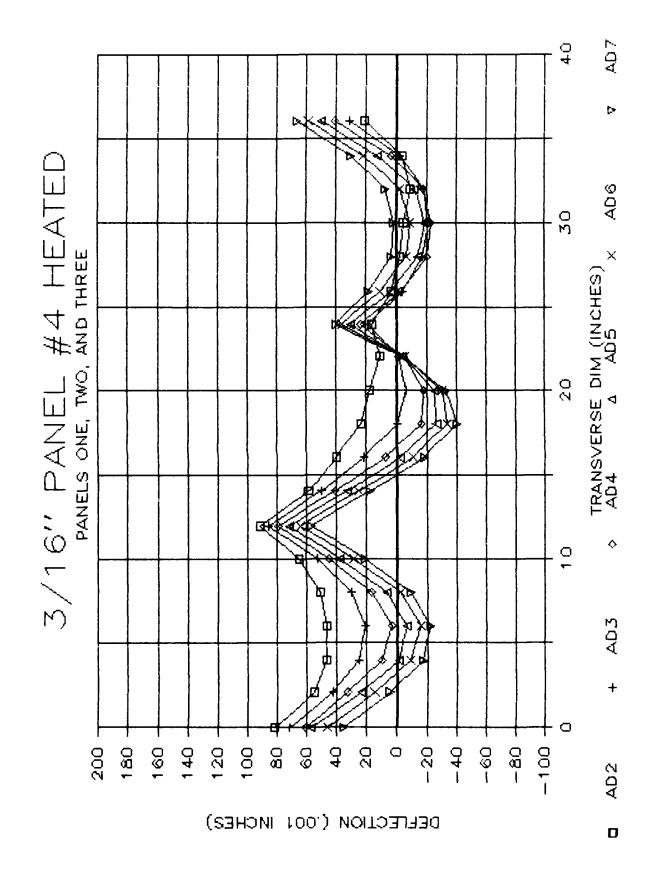
The horizontal coordinate is the transverse displacement. measured in inches. and the vertical coordinate is out-of-plane deflection. measured in thousandths of an inch.

Sykkelymeri isobabba bereserely asbabba isobases proposes passaces parafer passace passace bees N

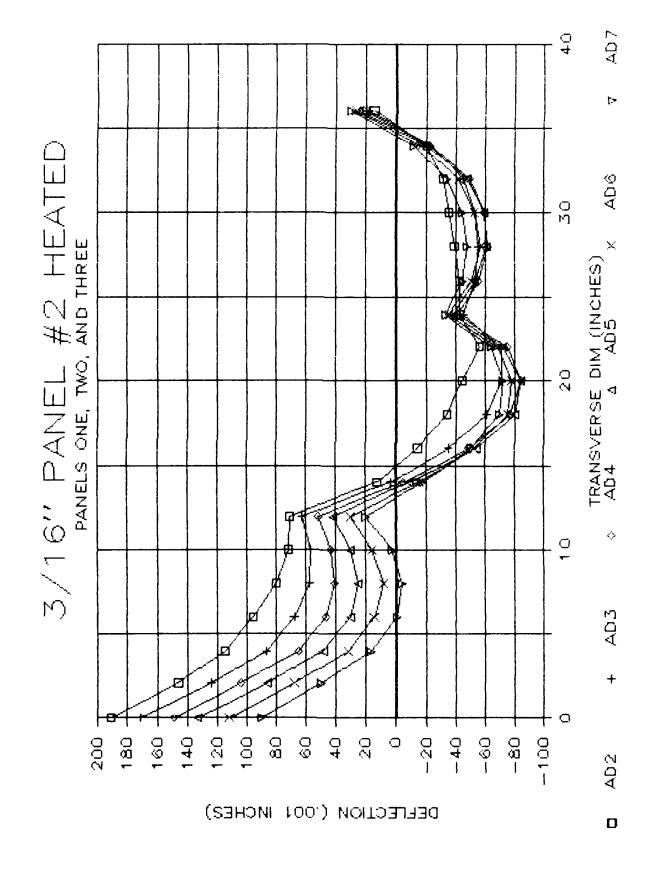


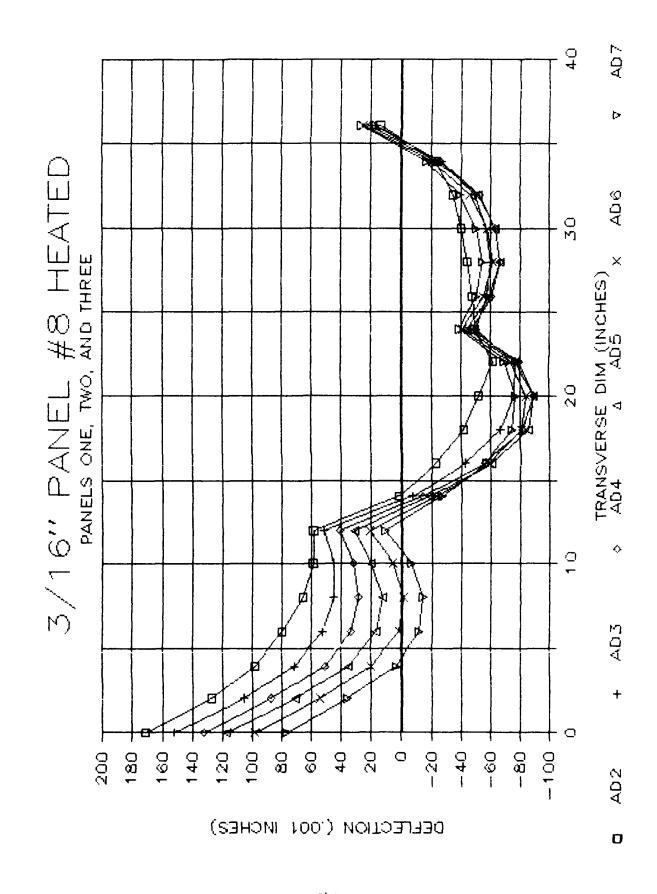
THE PROPERTY OF THE PROPERTY O

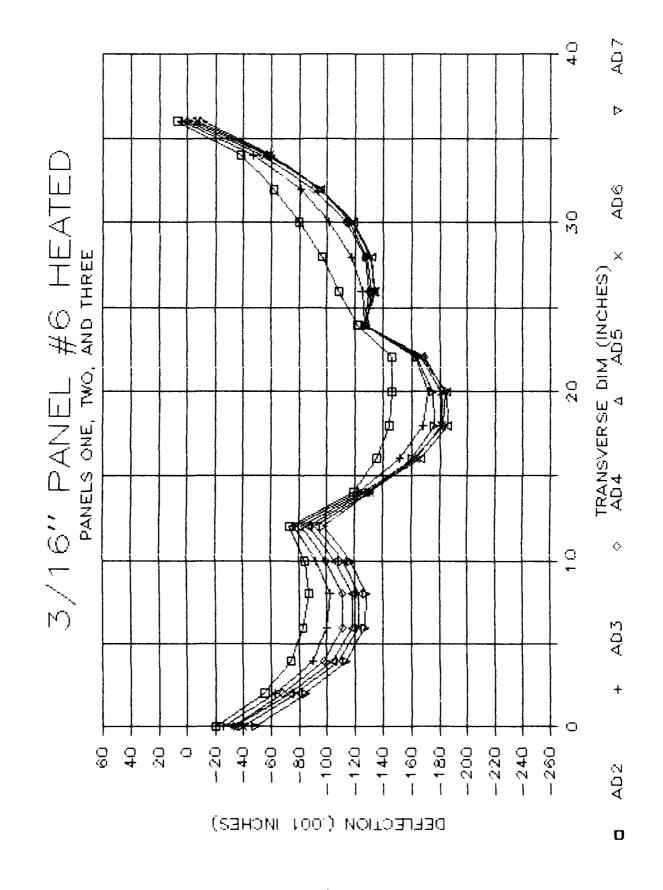




RECORDS RESERVED BUSINESS SANDARY INCOMESSION OF THE PROPERTY OF THE PROPERTY







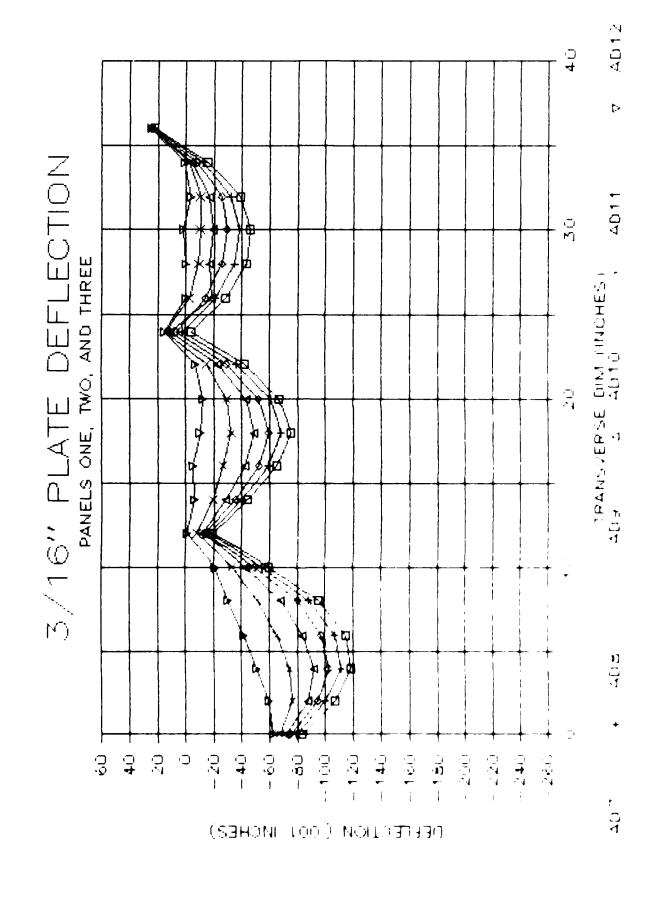
Kerkeren doddoor bissississin doorda birdoo boord

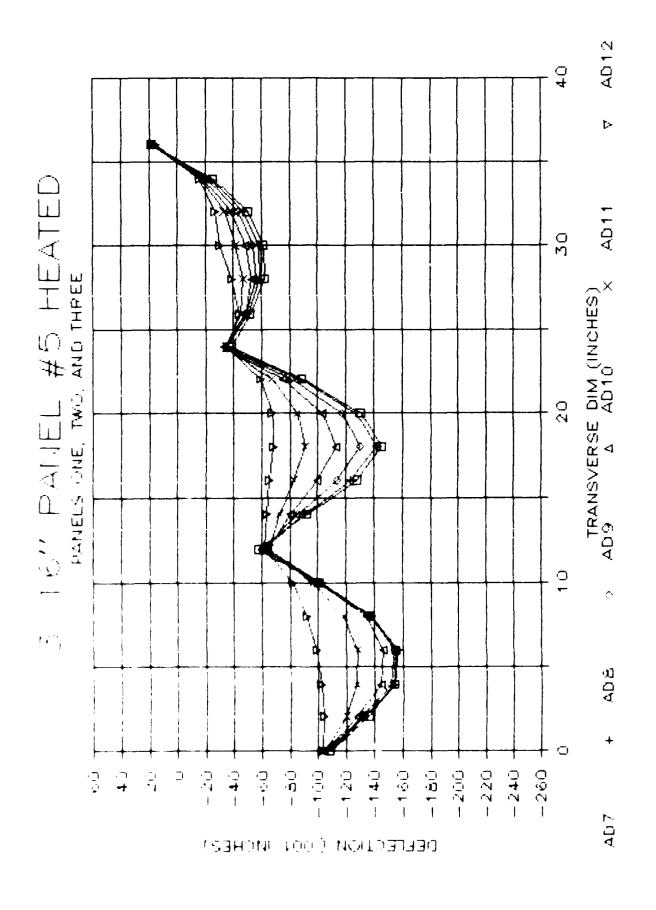
APPENDIX N

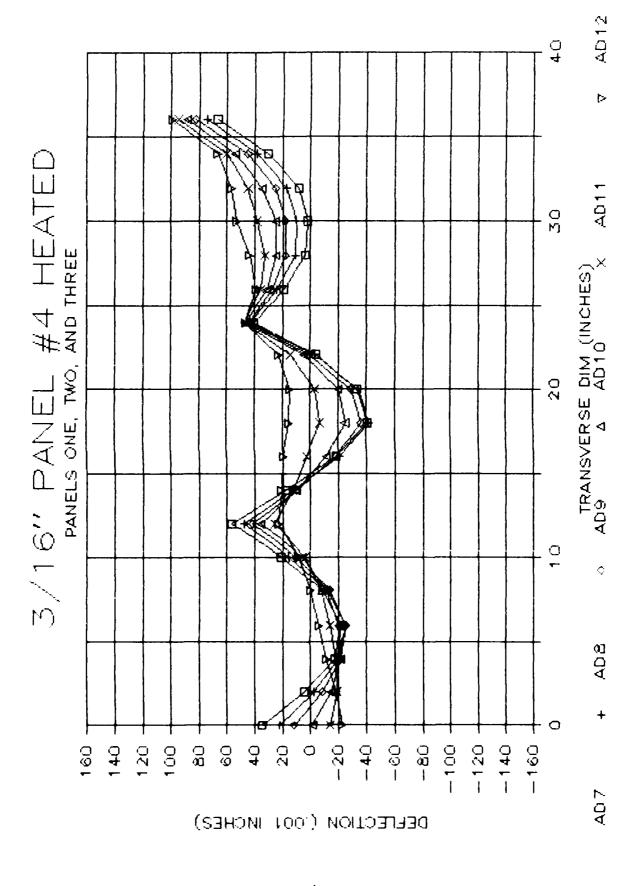
GRAPHS OF THE 3/16" STIFFENED PLATE TRANSVERSE OUT-OF-PLANE DEFLECTION READINGS FOR LINES AD7 THROUGH AD12

The horizontal coordinate is the transverse displacement. measured in inches, and the vertical coordinate is out-of-plane deflection, measured in thousandths of an inch.

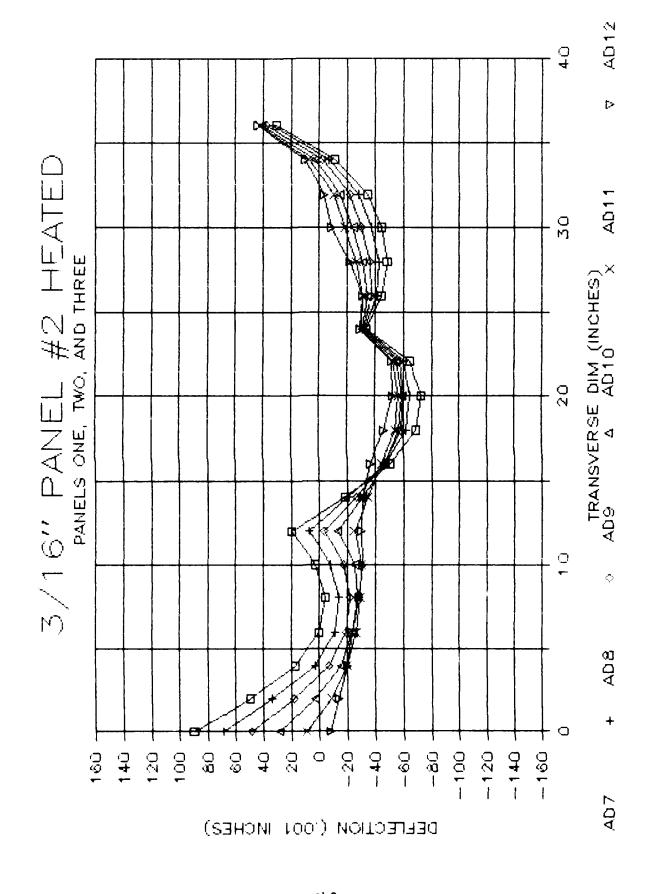
genes Ferences Thereard Ference Properties (States States Sabbook Services Sabbook Services (See

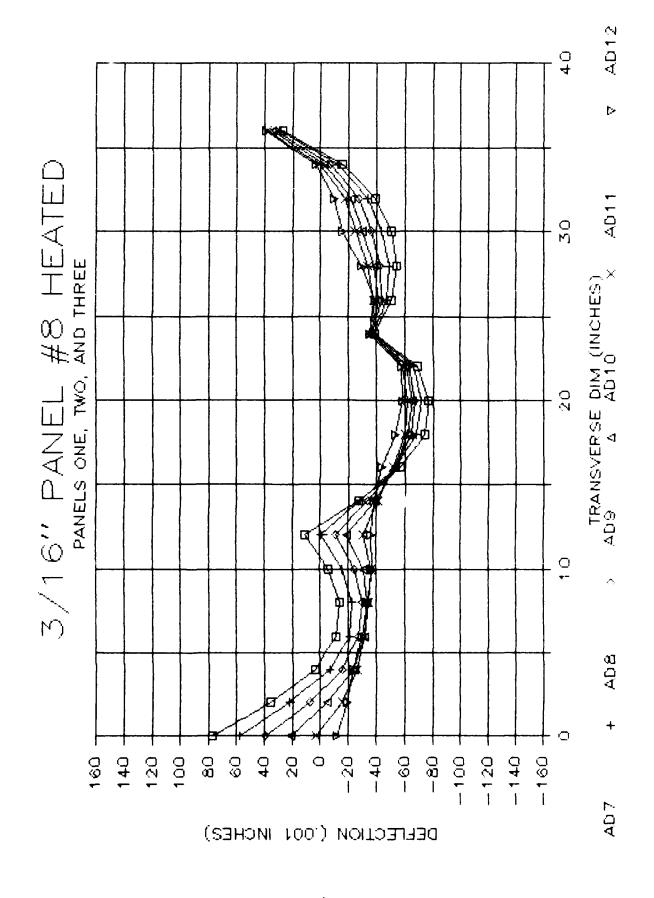




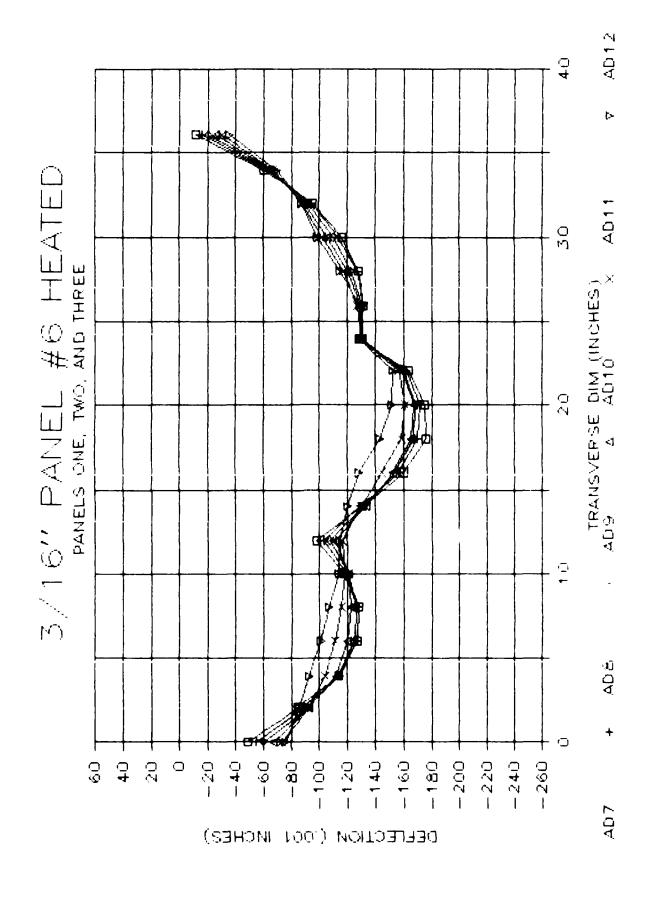


A SOLO COLO DE SOLO DE





reservation in the content of the co

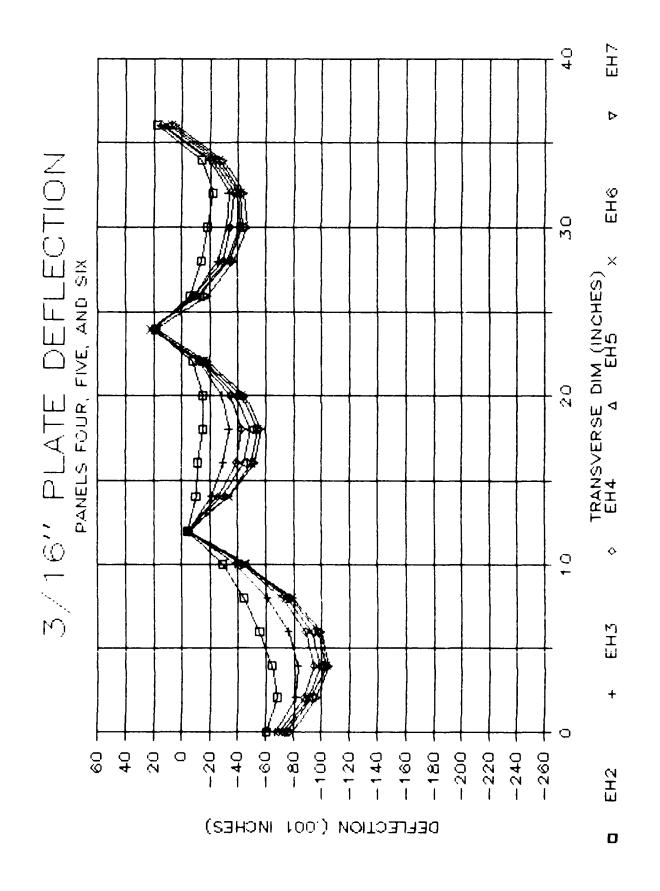


APPENDIX O

GRAPHS OF THE 3/16" STIFFENED PLATE TRANSVERSE OUT-OF-PLANE DEFLECTION READINGS FOR LINES EH2 THROUGH EH7

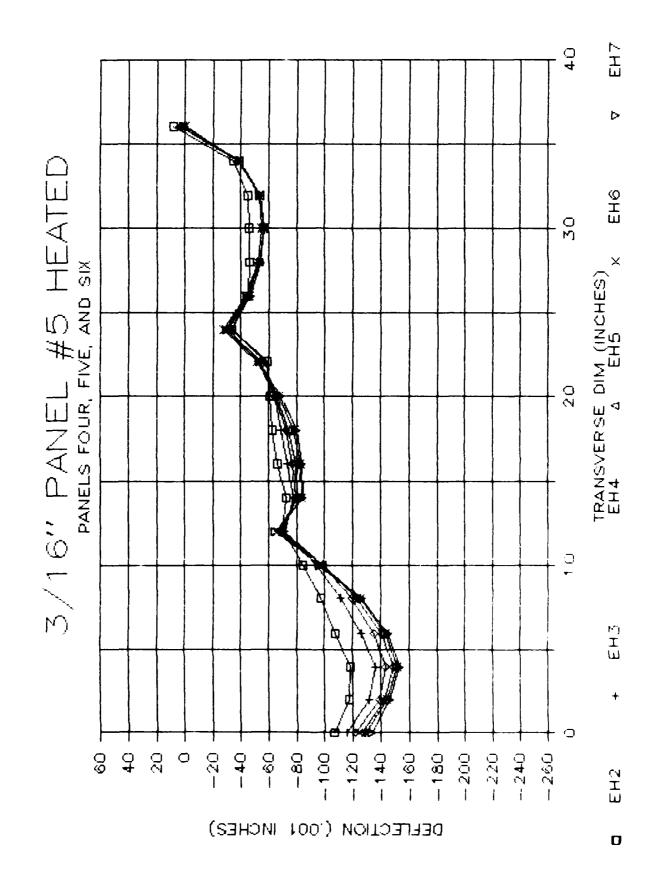
The horizontal coordinate is the transverse displacement, measured in inches, and the vertical coordinate is out-of-plane deflection, measured in thousandths of an inch.

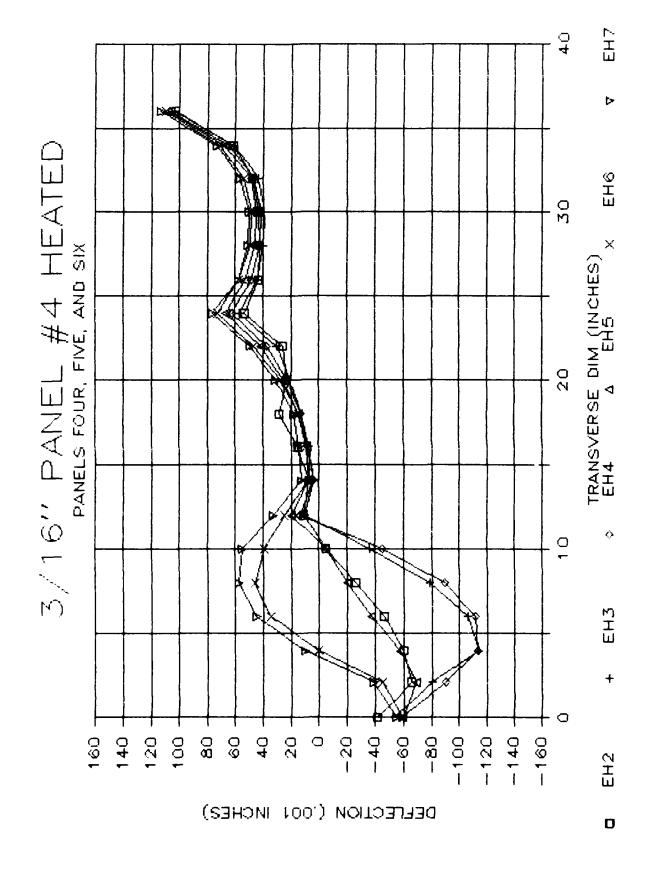
CONTRACTOR SESSESSES FOUNDED INSURANT COORDINATE CONTRACTOR SESSESSES FOUNDED INVESTIGATION OF THE PROPERTY OF



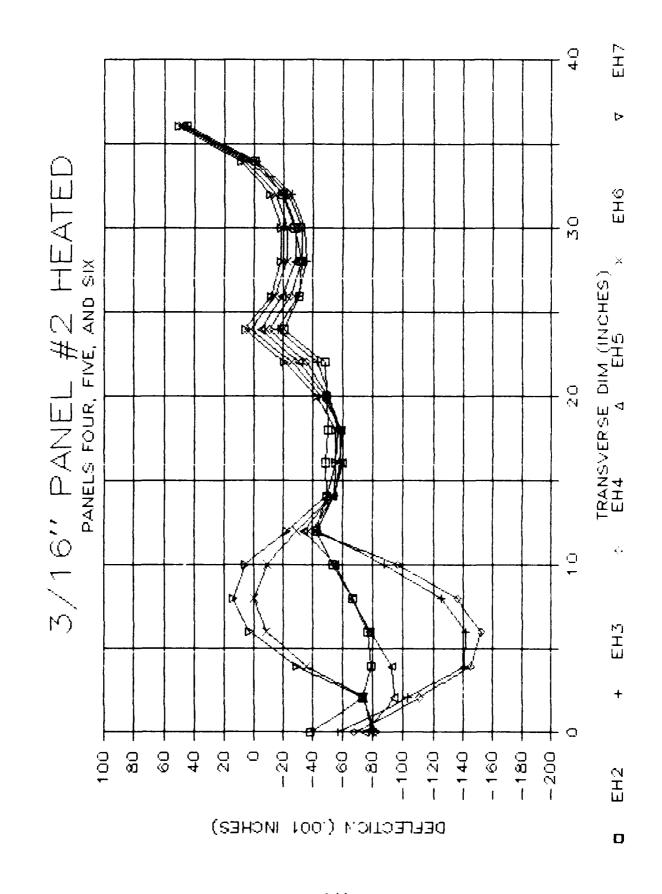
ALCOH PERCORE BURNEY SSENSE WASHIN VINNING

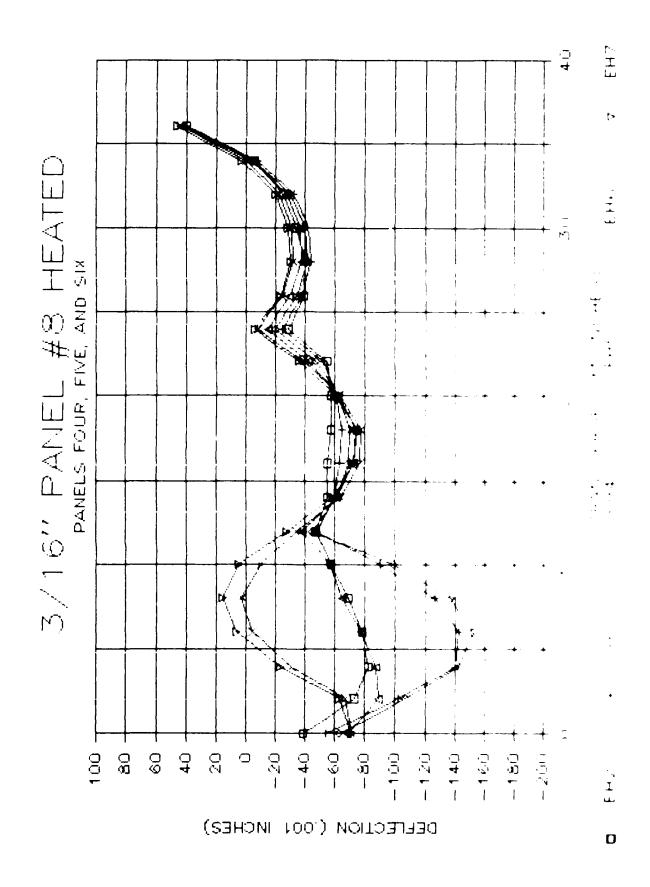
ではないとう。これのないが、これはないないでは、これのないない。これのないは、これのない。

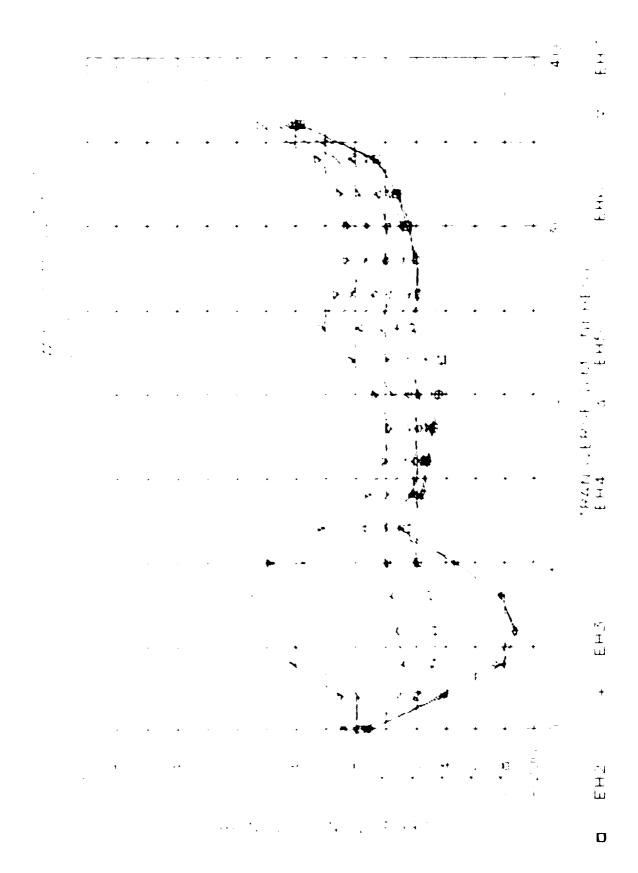




プログラング 一方の人のアング・アカルの人の人のできないがないがない。 アスピングライン 人のない



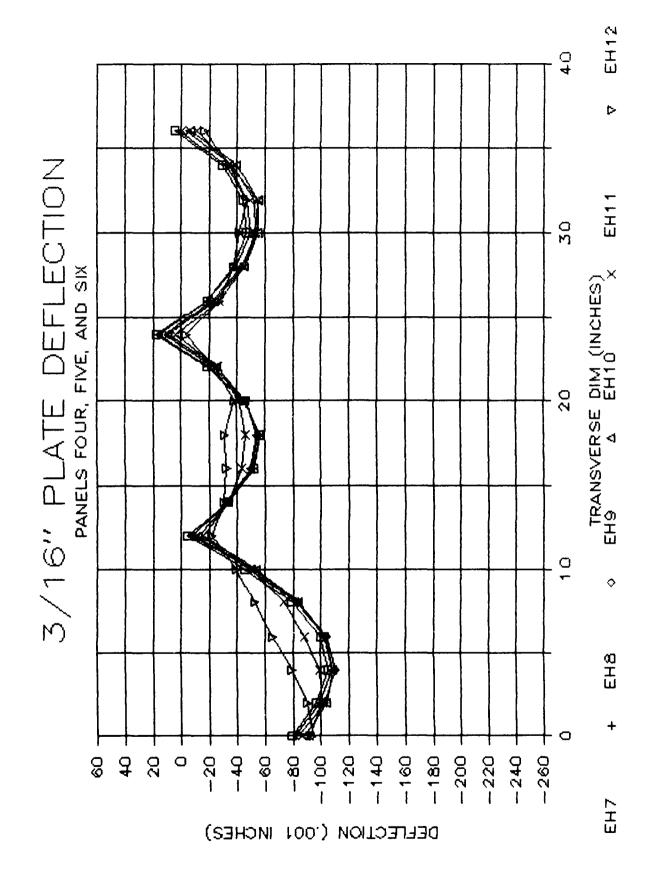


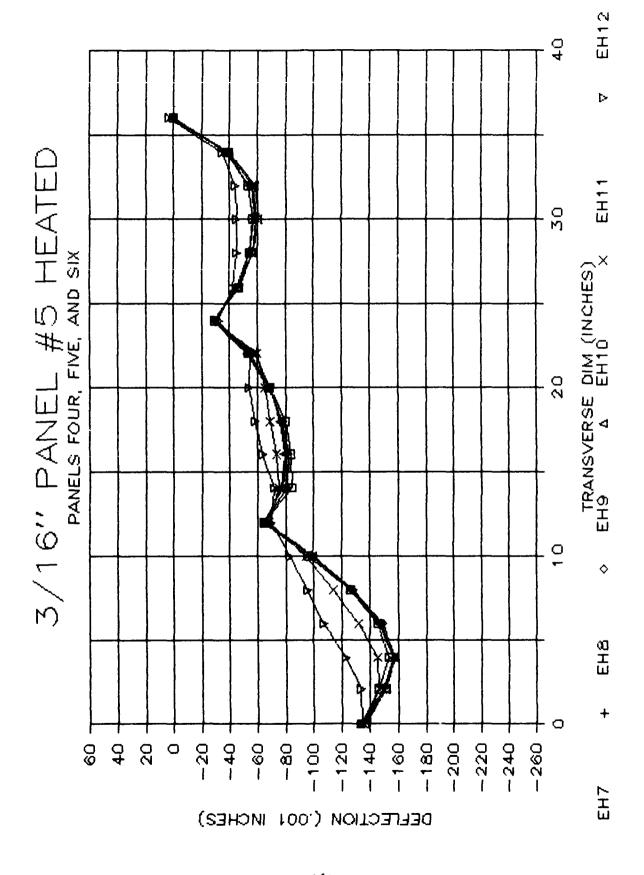


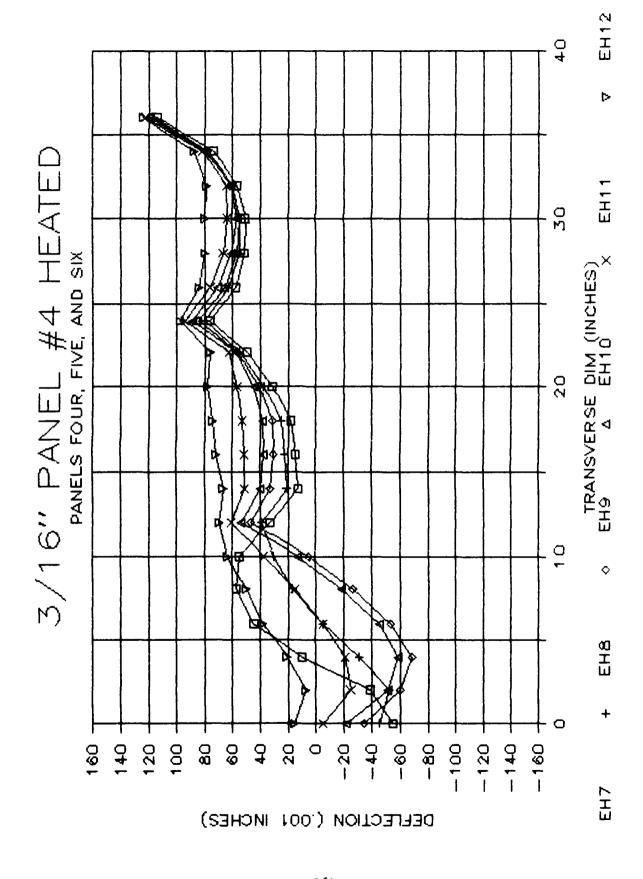
APPENDIX P

GRAPHS OF THE 3/16" STIFFENED PLATE TRANSVERSE OUT-OF-PLANE DEFLECTION READINGS FOR LINES EH7 THROUGH EH12

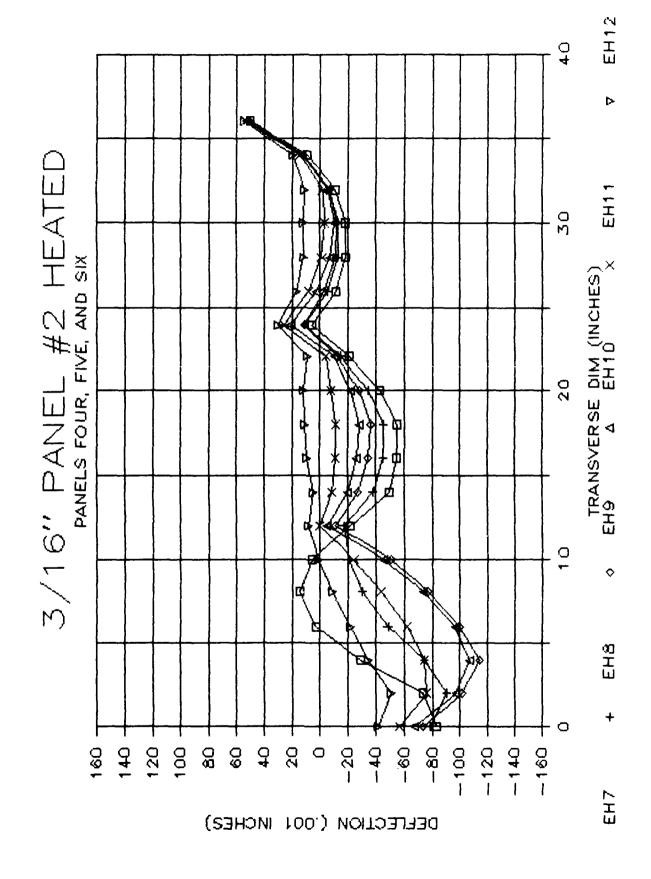
The horizontal coordinate is the transverse displacement. measured in inches. and the vertical coordinate is out-of-plane deflection. measured in thousandths of an inch.

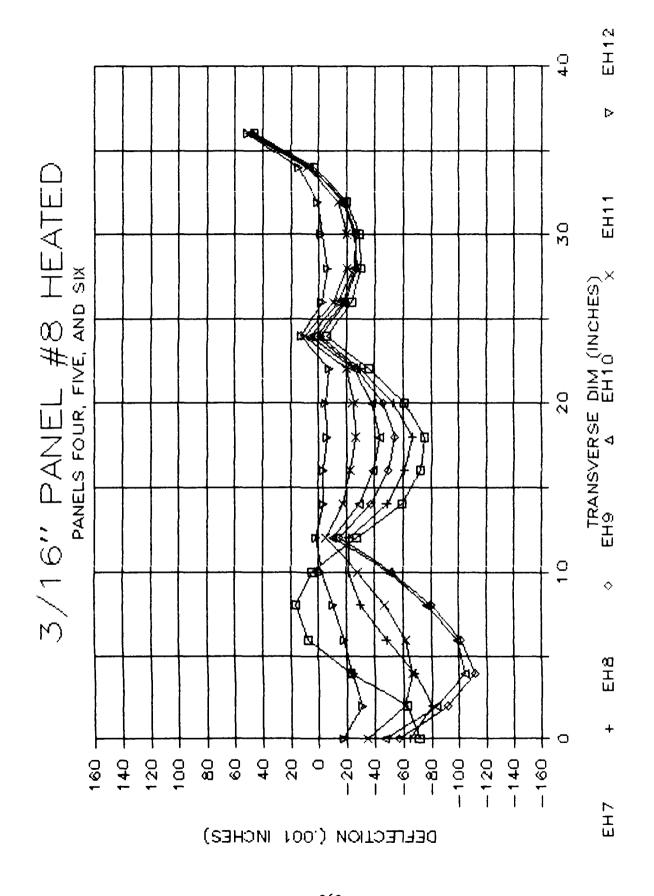


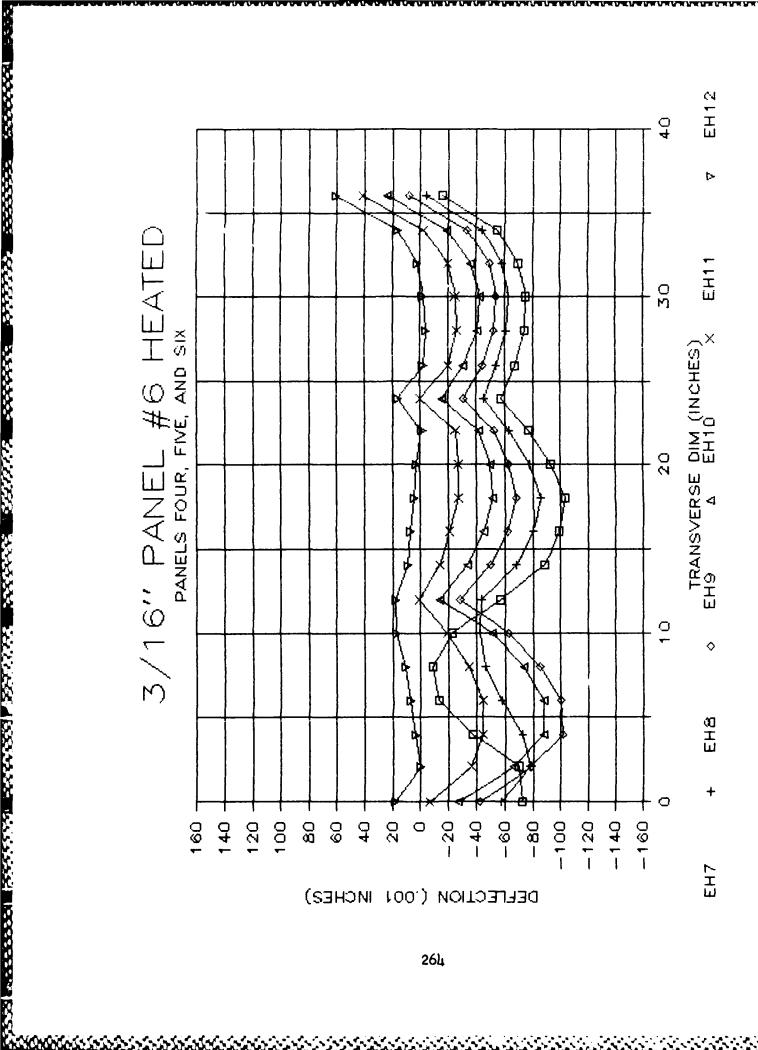




TO SELECTION TO SELECT THE SECRETARY OF THE SECRETARY OF



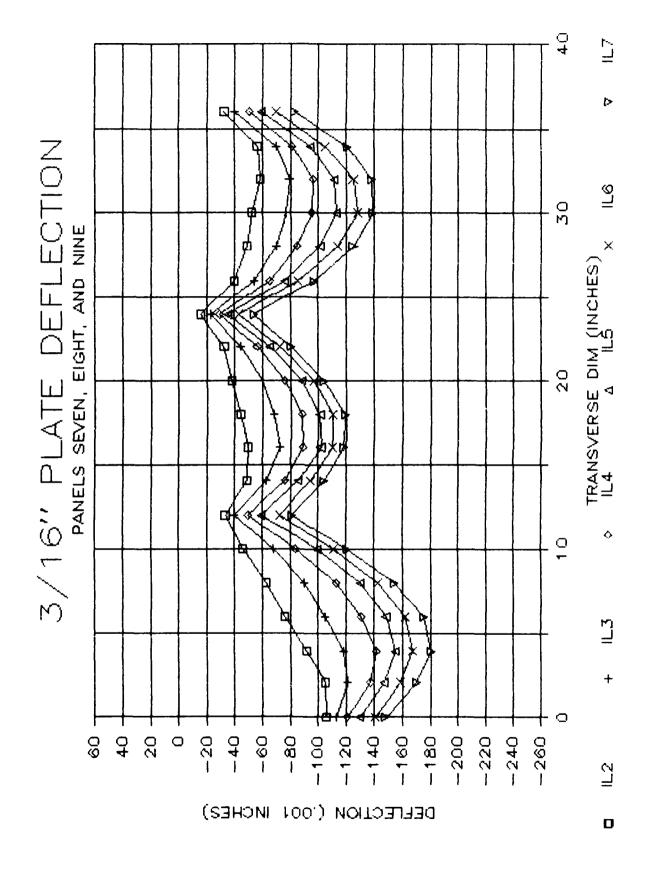


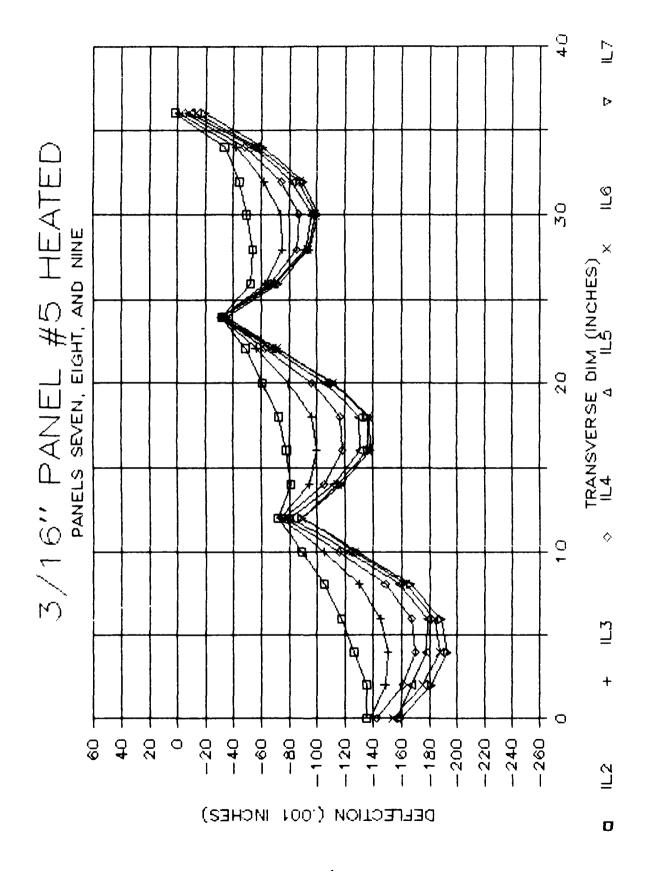


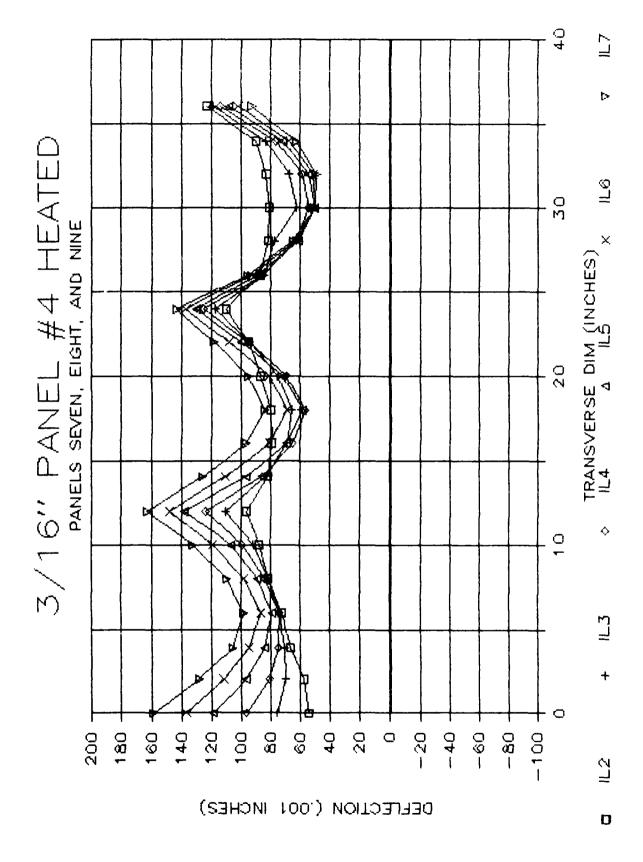
APPENDIX 0

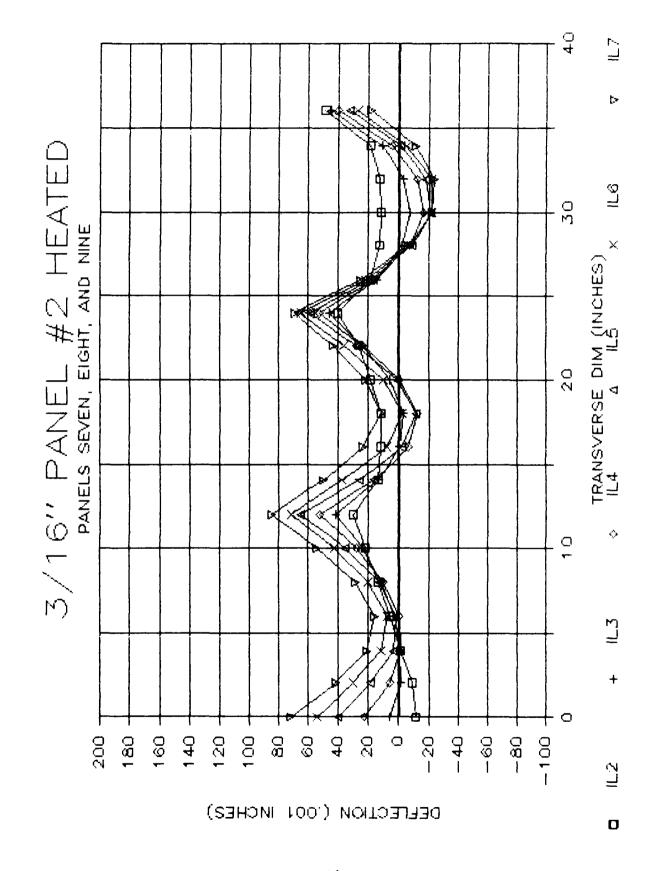
GRAPHS OF THE 3/10" STIFFENED PLATE TRANSVERSE
OUT-OF-PLANE DEPLECTION READINGS FOR LINES
112 THROUGH IL7

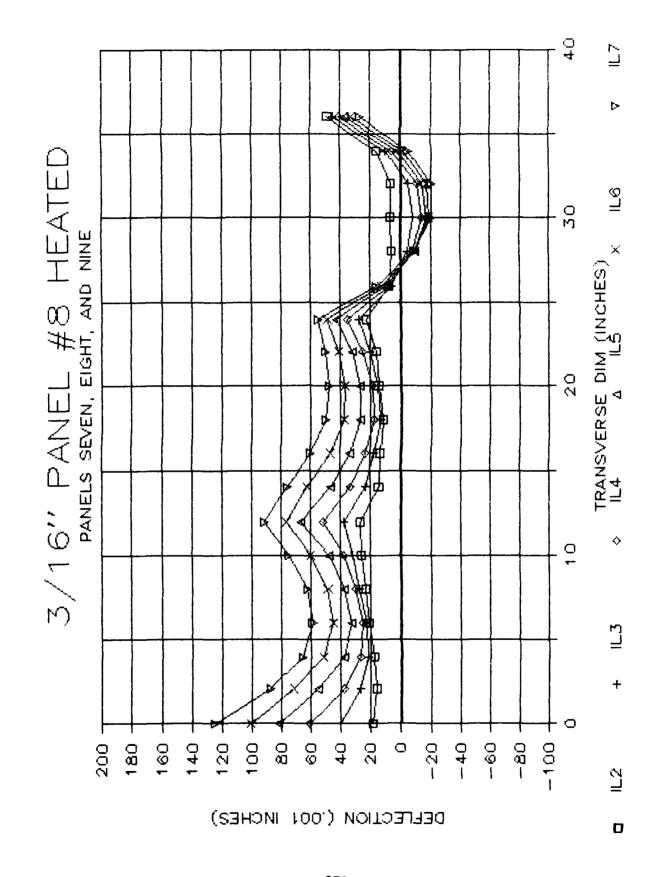
The horizontal coordinate is the transverse displacement.
measured in inches, and the vertical coordinate is out-ofplane deflection, measured in thousandths of an inch.



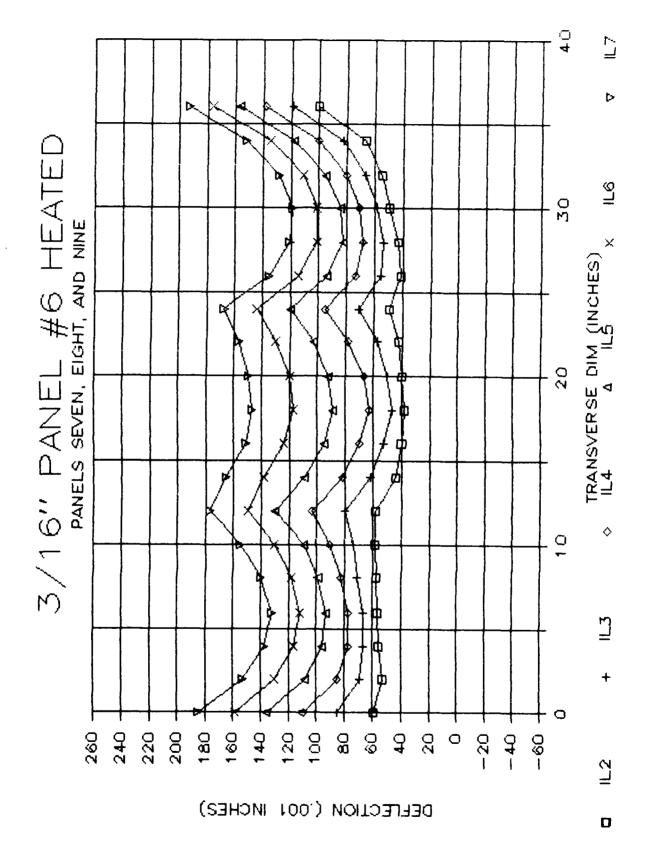








KAMPERSON ESPECIAL EXPERIENTED STRING ESTITION EXPERIS ESTITION ESTITION OF THE PROPERTY OF TH

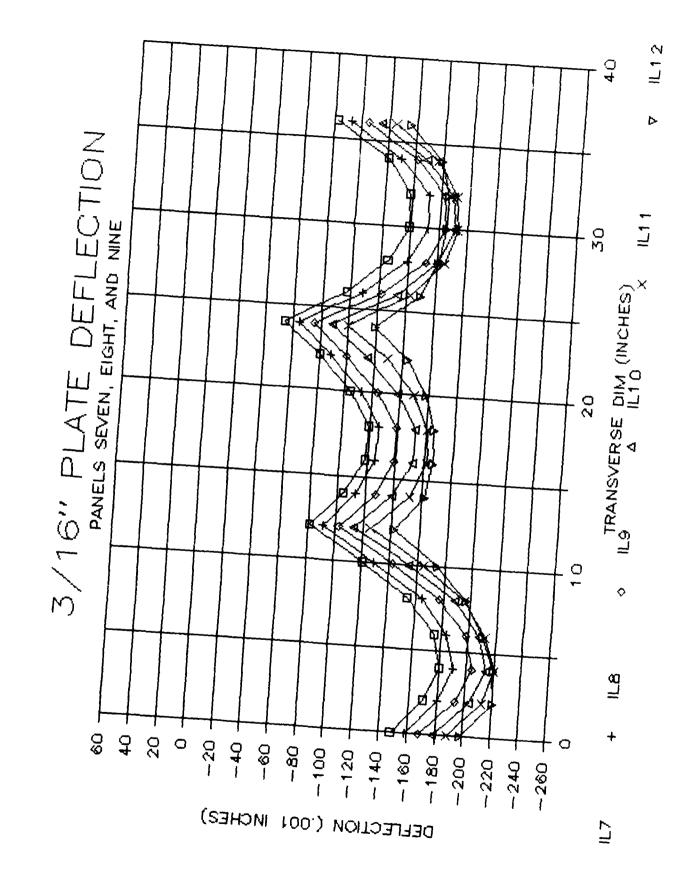


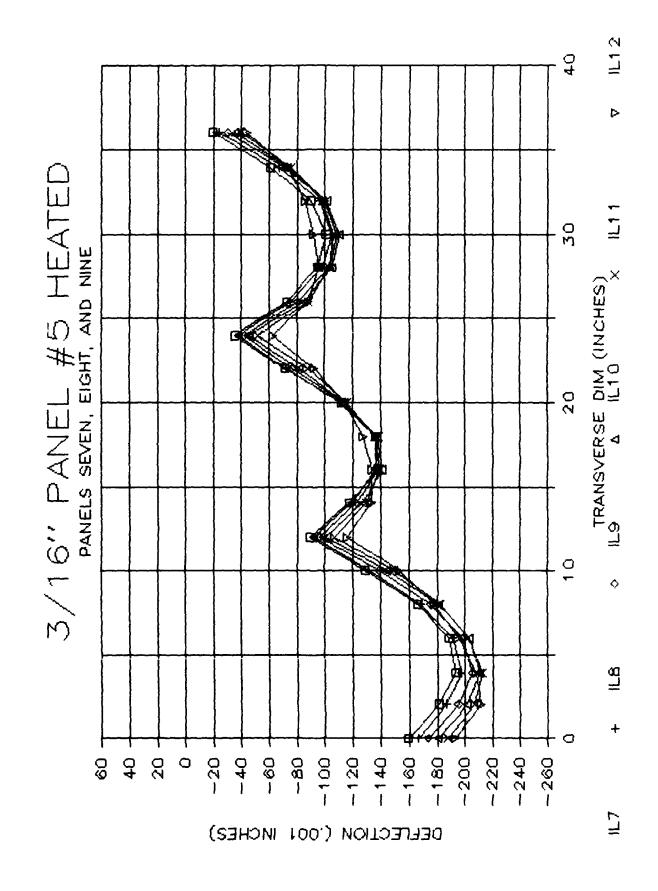
general societies contrated and the contrate societies are an expected assessed assessed and an expected and a

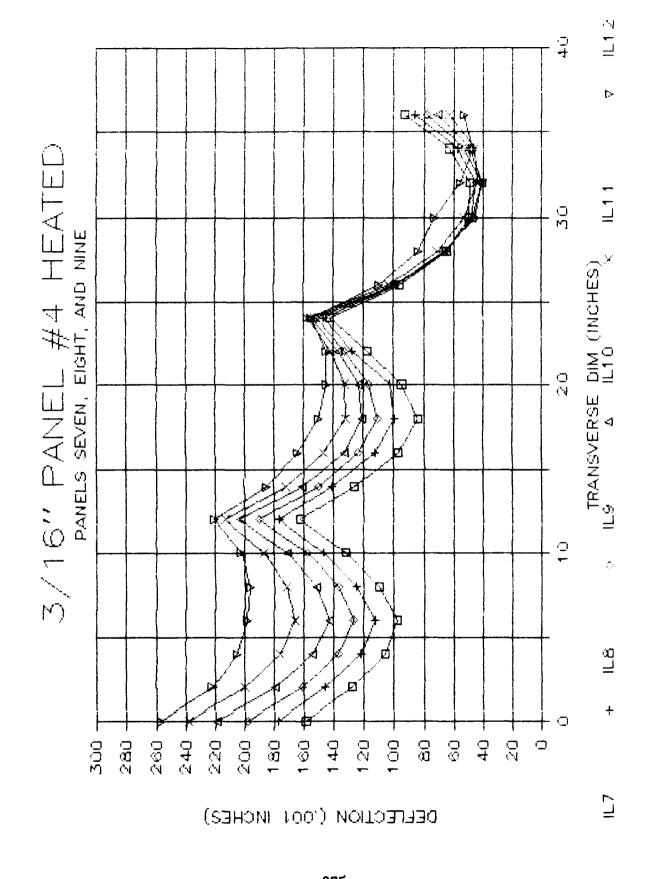
APPENDIX R

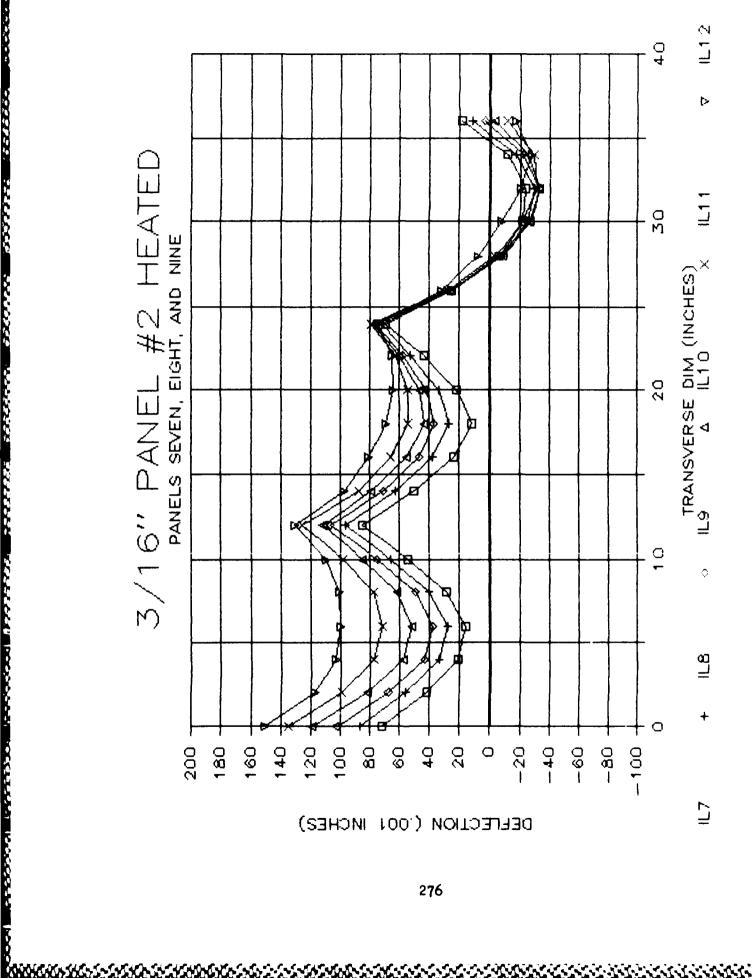
GRAPHS OF THE 3/16" STIFFENED PLATE TRANSVERSE OUT-OF-PLANE DEFLECTION READINGS FOR LINES IL7 THROUGH IL12

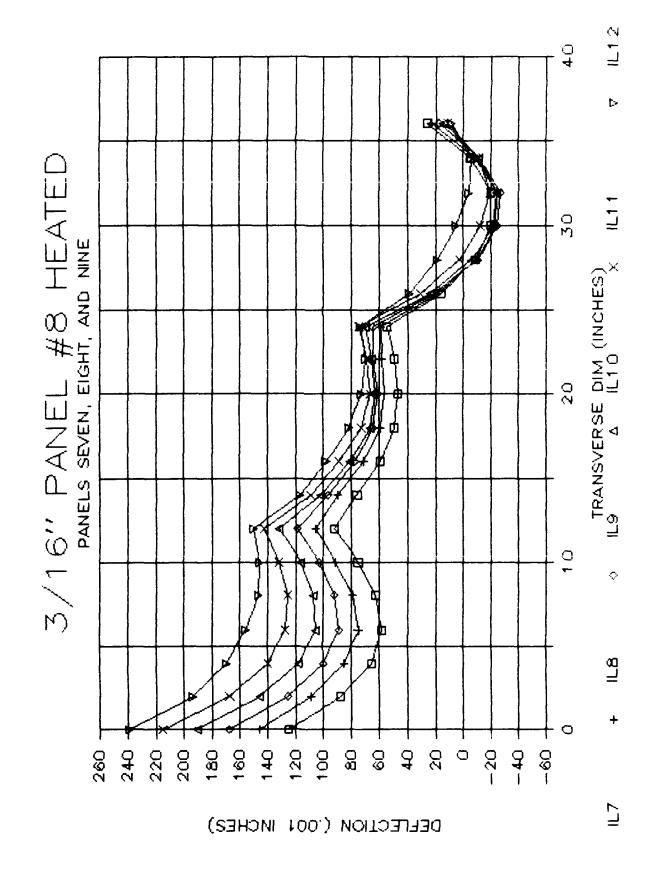
The horizontal coordinate is the transverse displacement. measured in inches. and the vertical coordinate is out-of-plane deflection, measured in thousandths of an inch.



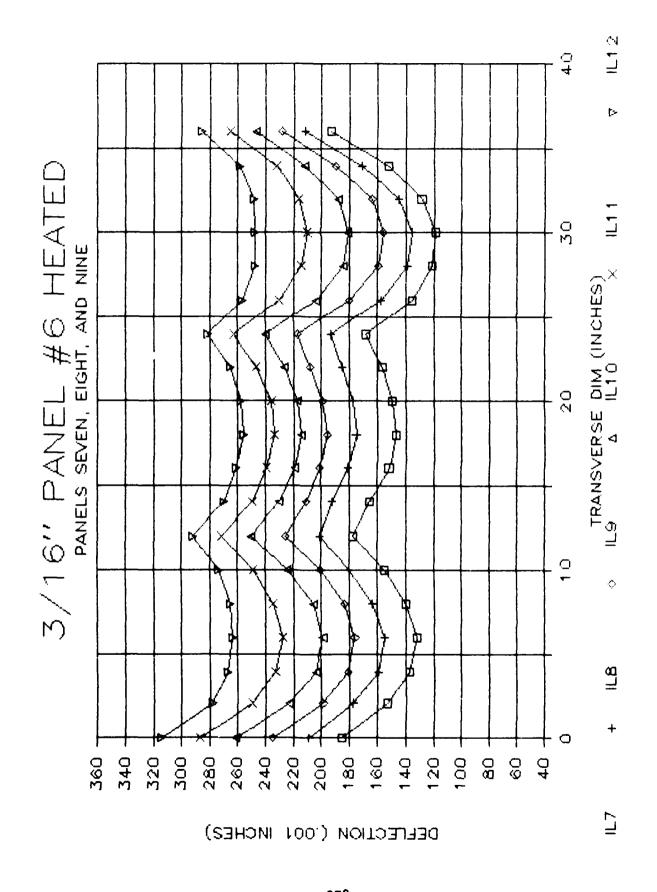








PROPERTY AND PROPE

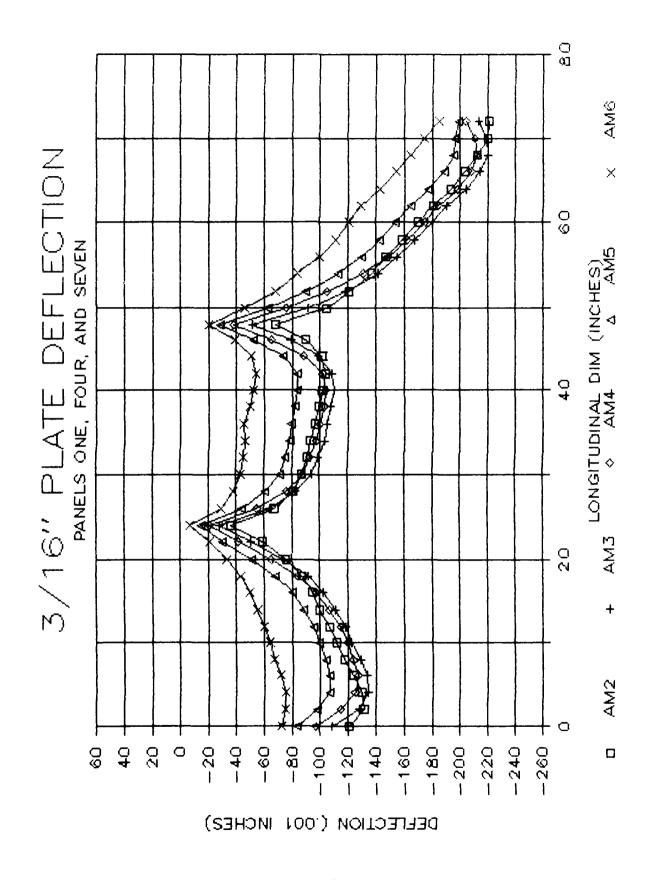


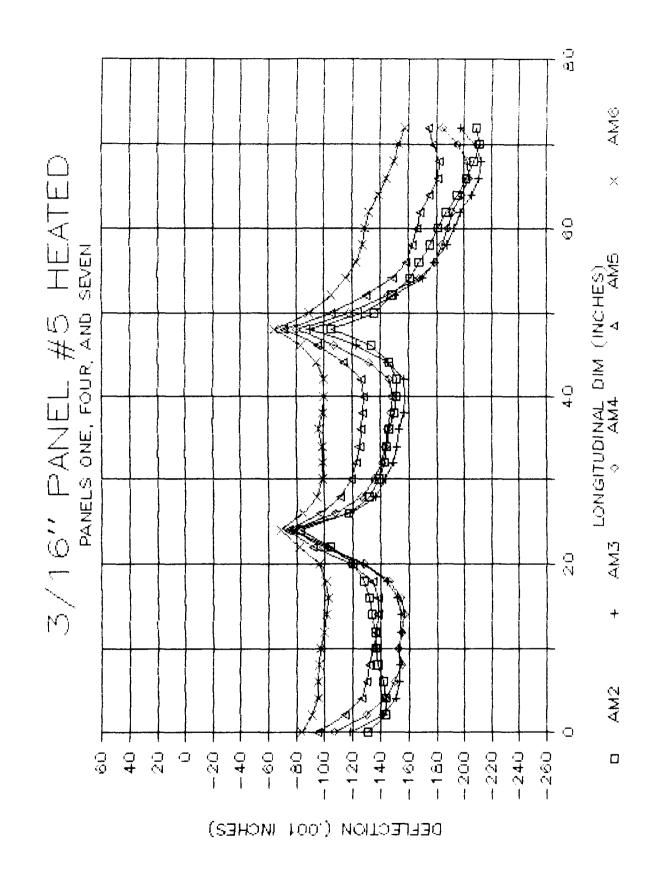
CONTRACT STATES CONTRACT STATES INCOME.

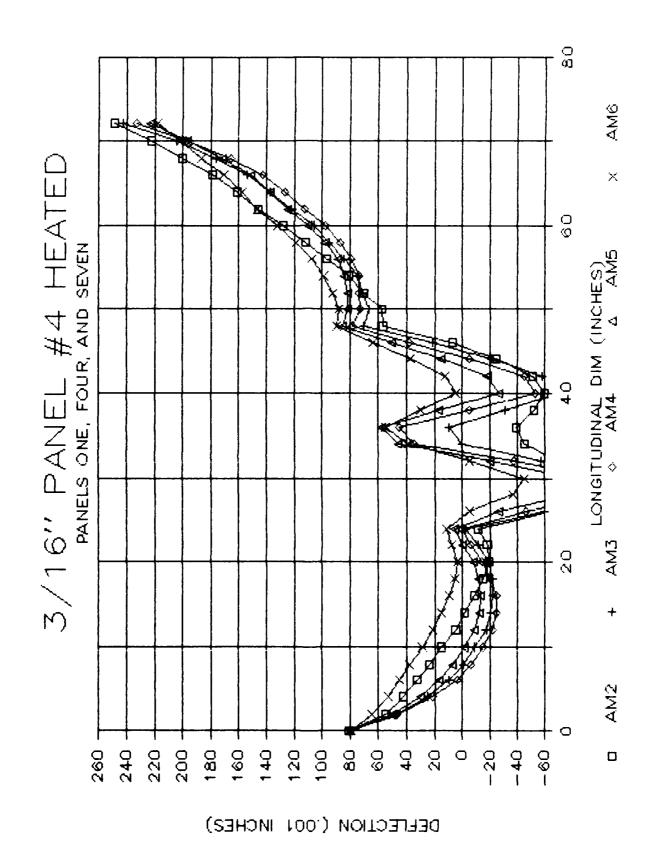
APPENDIX S

GRAPHS OF THE 3/16" STIFFENED PLATE LONGITUDINAL OUT-OF-PLANE DEFLECTION READINGS FOR LINES AM2 THROUGH AM6

The horizontal coordinate is the longitudinal displacement, measured in inches, and the vertical coordinate is out-of-plane deflection, measured in thousandths of an inch.

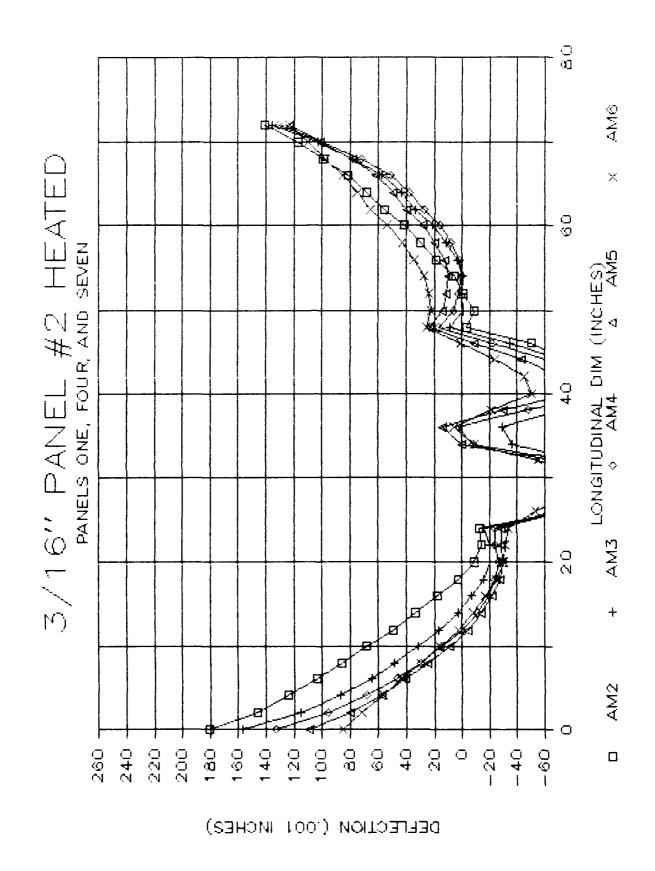


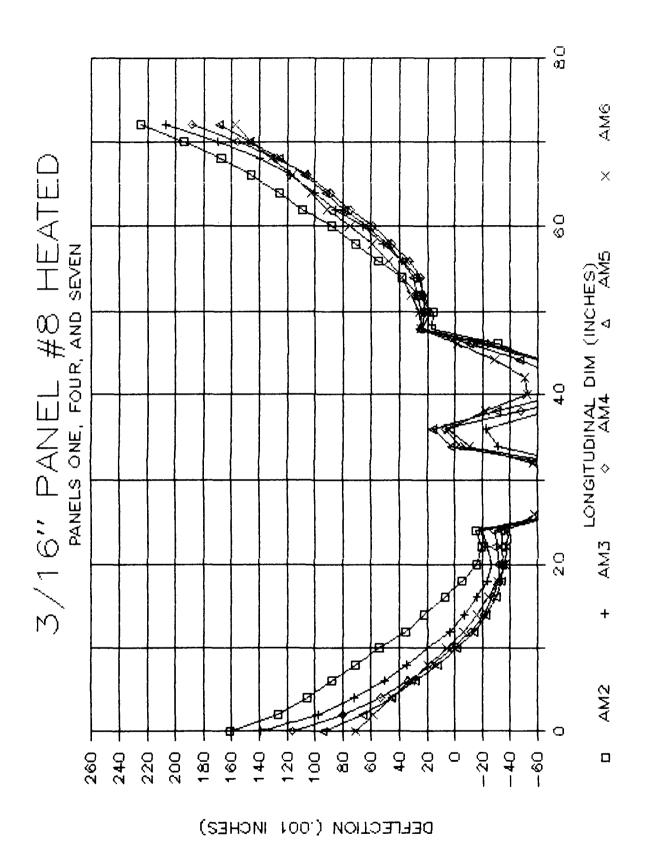




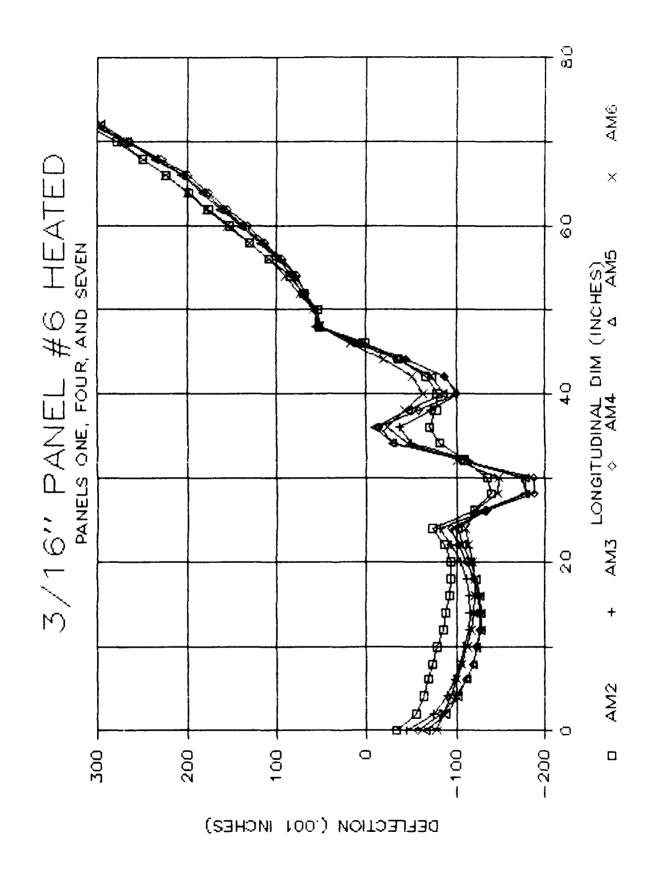
STATE PROPERTY CONSISSES BYTHERY CONSISSES

PRODUCE RESERVANT ADDITIONAL LOCALISMS AND SERVICE RECORD





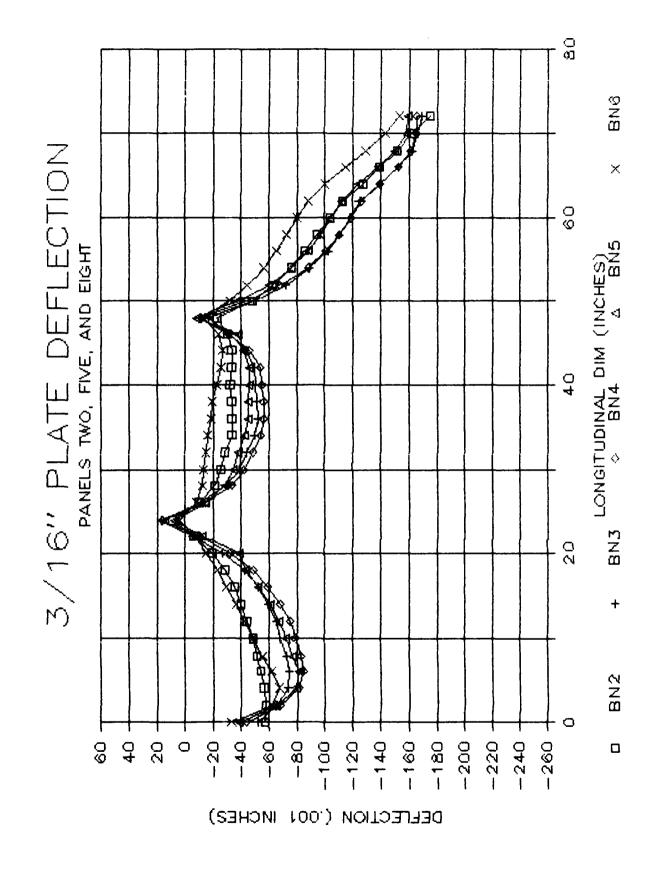
がたびのあるようなものできないないないないのできないないないないないない。例じくくくんしては関するかのないのであるのといる。 関われたいない 関係を含める かん 関節なる ちょうかい

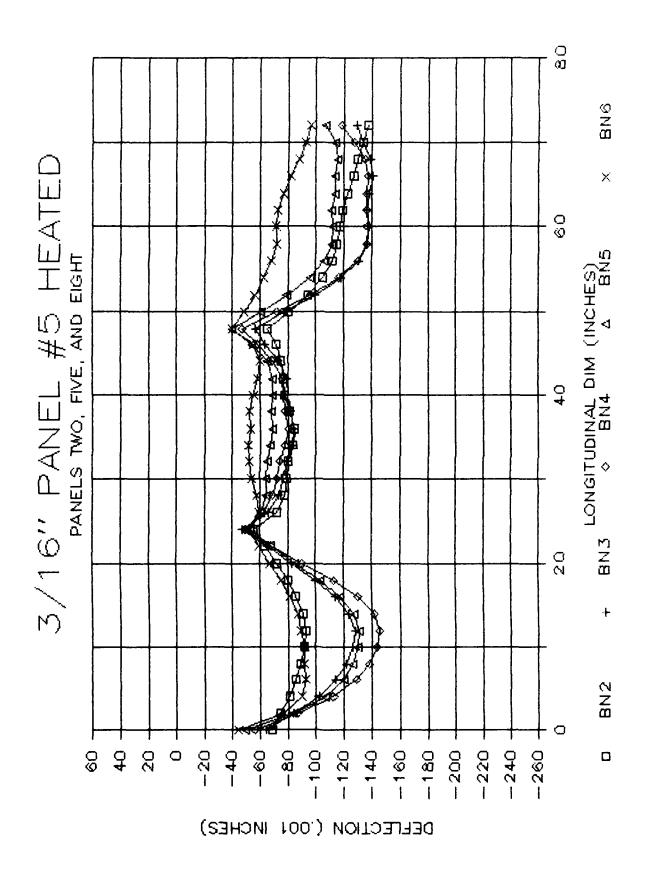


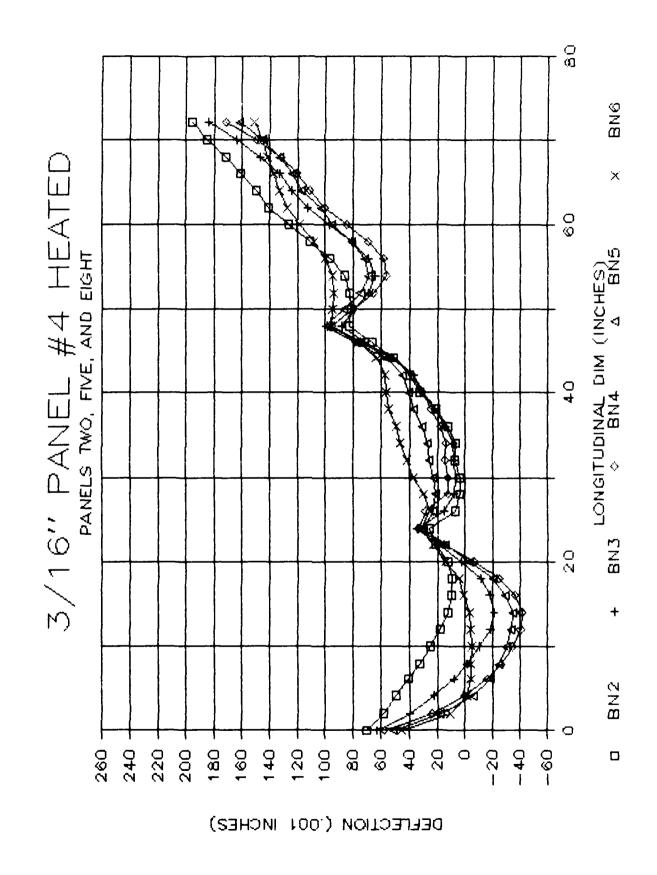
APPENDIX T

GRAPHS OF THE 3/16" STIFFENED PLATE LONGITUDINAL OUT-OF-PLANE DEFLECTION READINGS FOR LINES BN2 THROUGH BN6

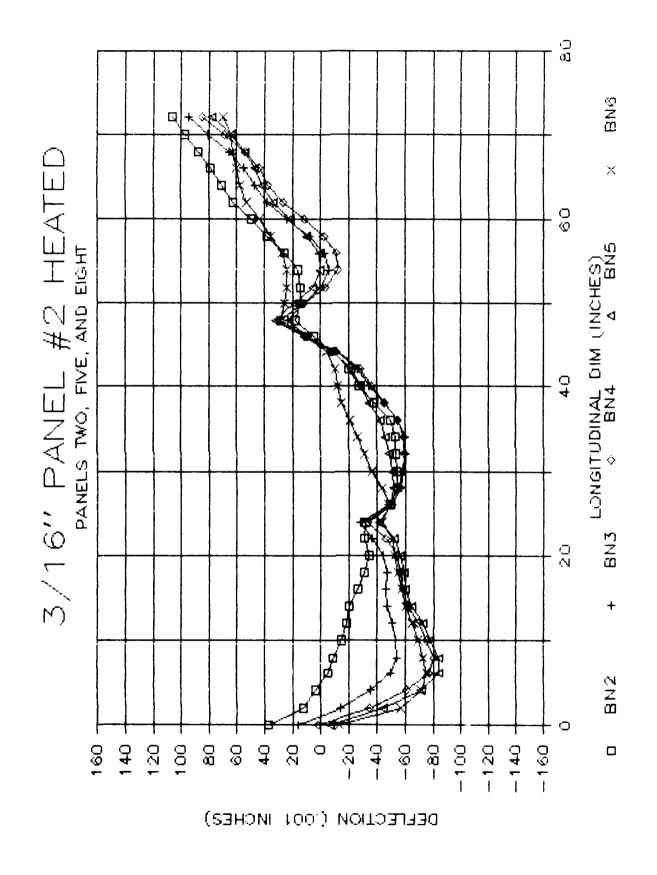
The horizontal coordinate is the longitudinal displacement, measured in inches, and the vertical coordinate is out-of-plane deflection, measured in thousandths of an inch.

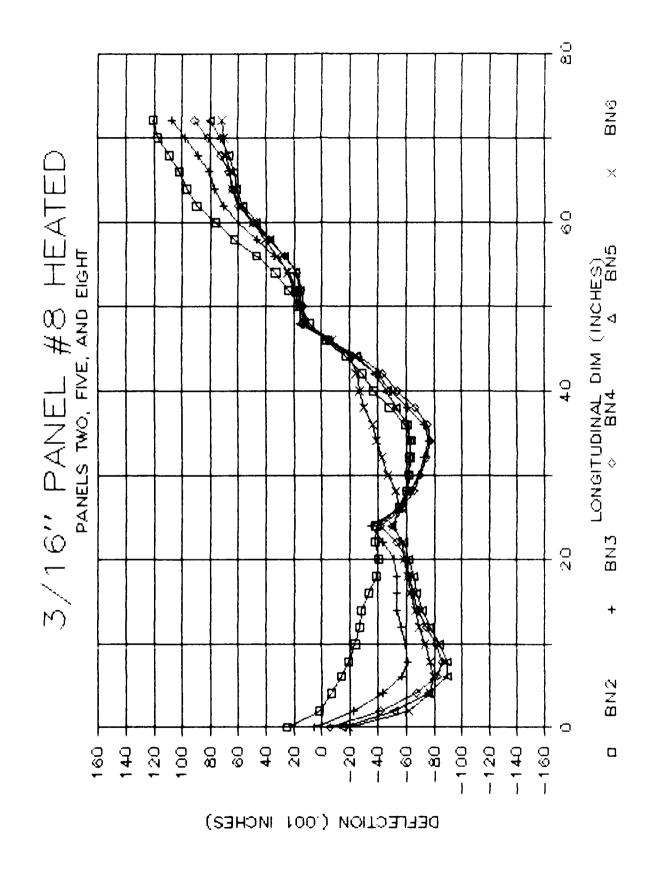


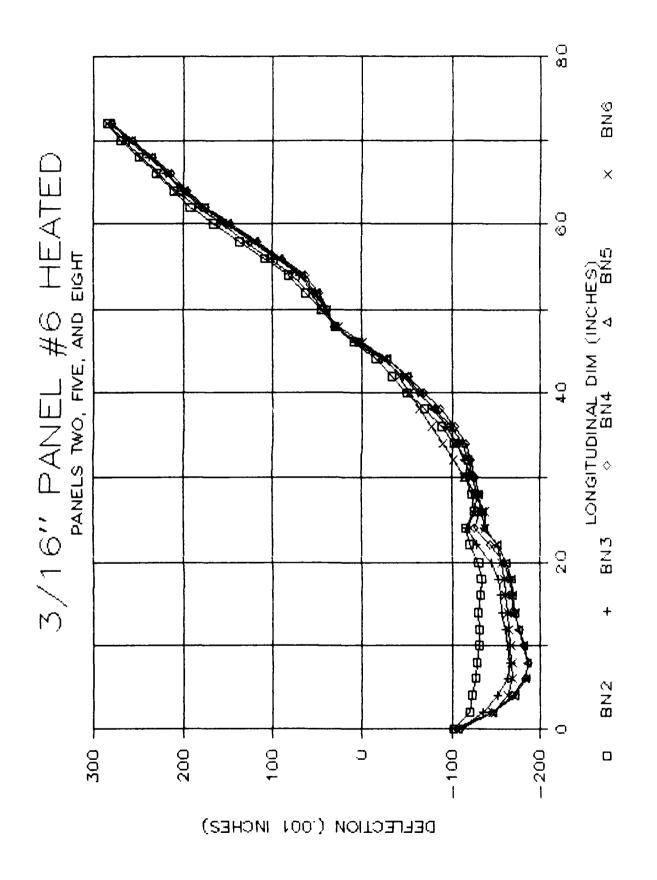




PANASSA ROSTON STANDS CAMERON SERVING MINNEY ASSAULT



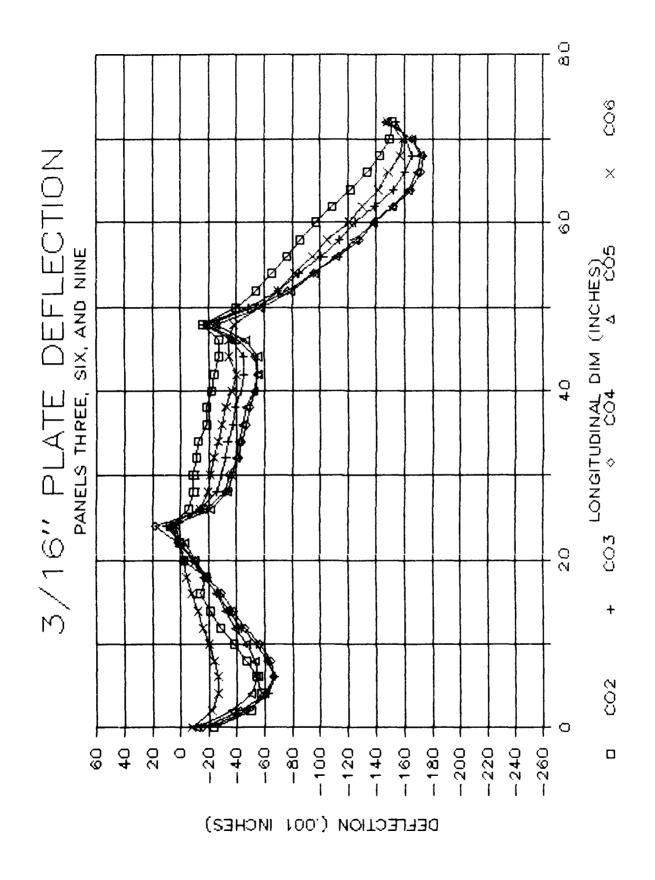


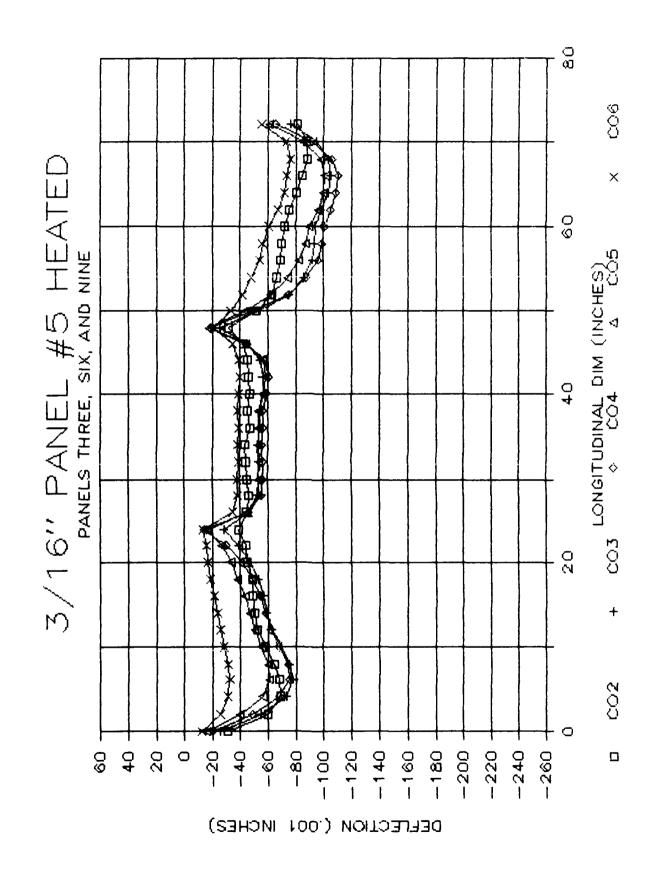


APPENDIX U

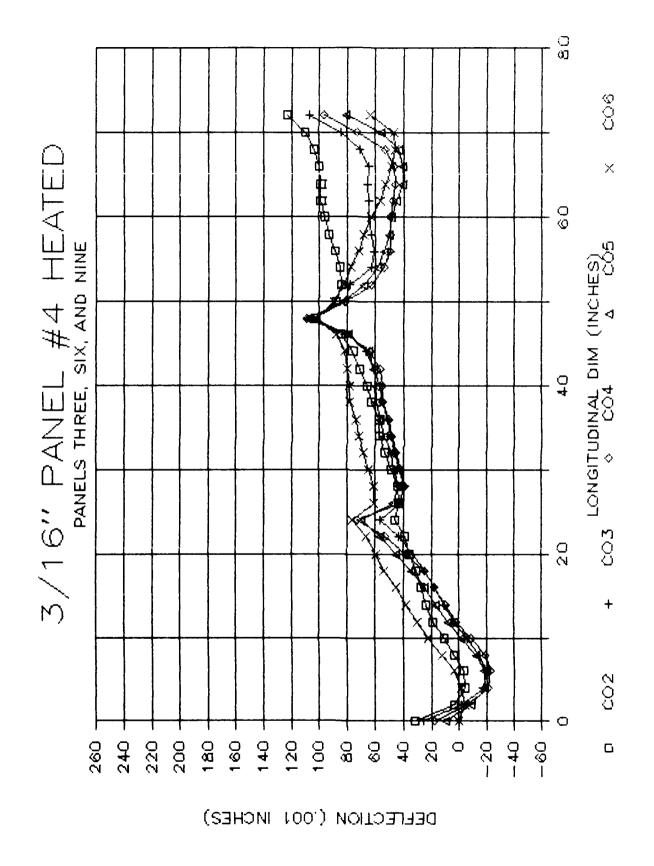
GRAPHS OF THE 3/16" STIFFENED PLATE LONGITUDINAL OUT-OF-PLANE DEFLECTION READINGS FOR LINES CO2 THROUGH CO6

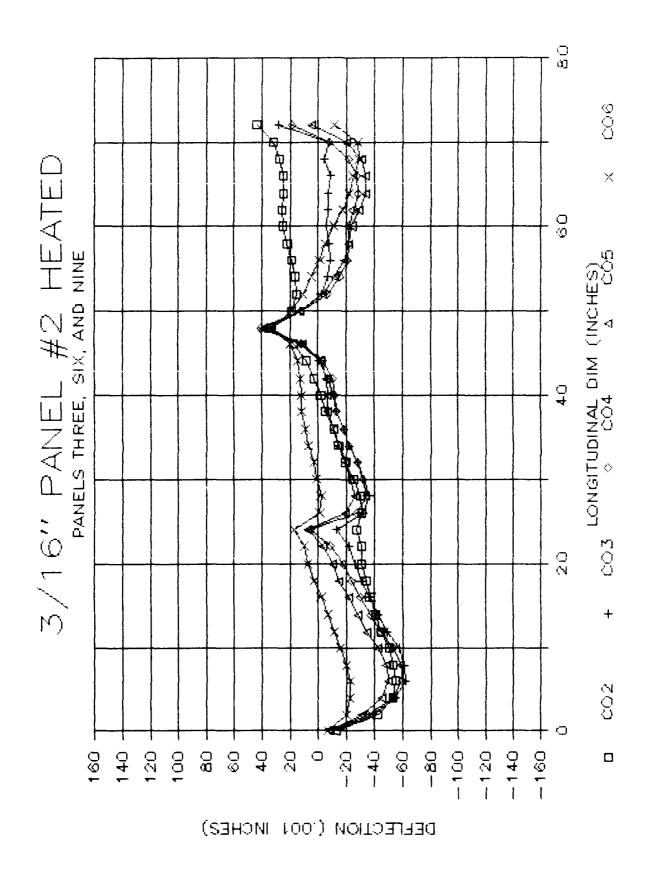
The horizontal coordinate is the longitudinal displacement, measured in inches, and the vertical coordinate is out-of-plane deflection, measured in thousandths of an inch.

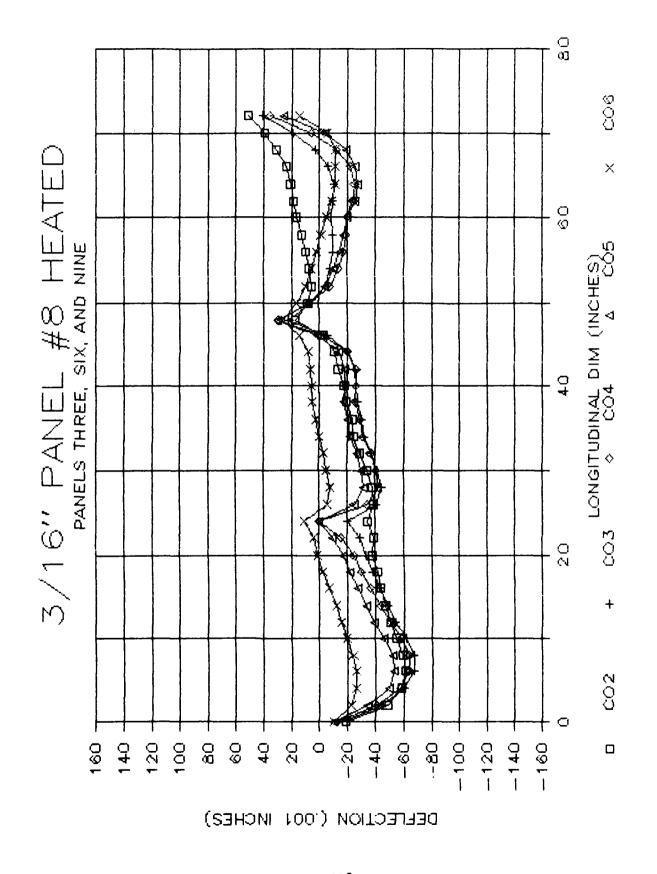


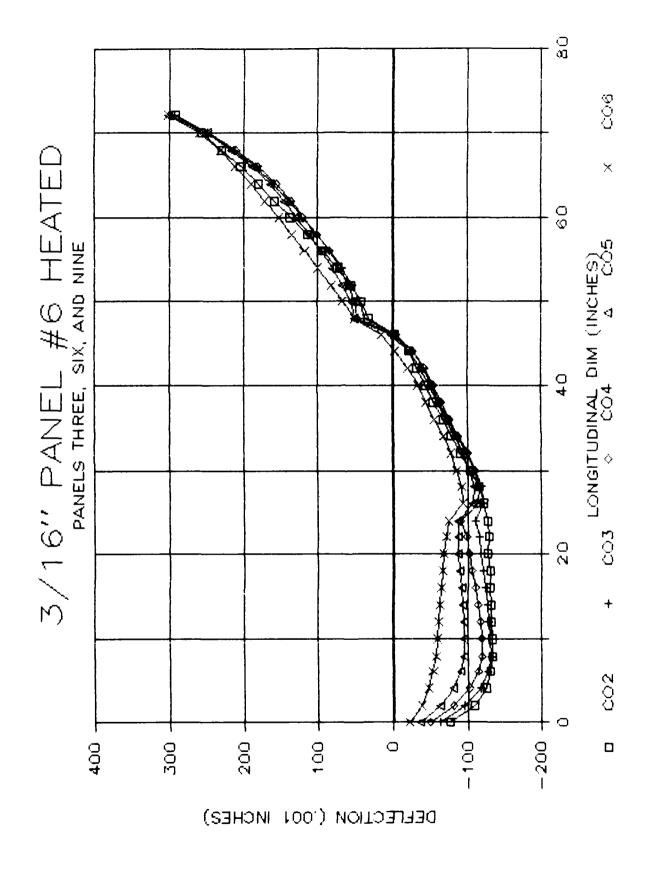


resear provides offerease expressed research against









APPENDIX V

3/16" STIFFENED PLATE MID-PANEL DEFLECTION DATA D(MAX)iT AND D(MAX)iL

This appendix contains the mid-panel deflection data, D(MAX)iT and D(MAX)iL, for the 3/16" stiffened plate. The data is in tabular form. All deflection readings are in thousandths of an inch. See Figure 3-2 for the definition of D(MAX)iL.

3/16" FLATE
Out of plane deflection at the center of panel i. referenced to the transverse straight line connecting the mid points of that panel's longitudinal stiffeners. See Figure 3-2 for the Befinition of I(MAX)iT.

		PANEL		:	!	•	1	•	1	1 1	1
	ļΗ	EATED*	ID(MAX)1T	(1D(MAX)21	(LDC MAX)3T			1D(MAX)6T	D(NAX)7T	TB(XAK)QT	ID(HAX)9TI
	;-				·;	!	;	i			
	ŀ		1	1	1	!		: 			
F	;	WELD	63.5								
Ι	ŀ	#5	1 71.75								
R	i	#4	1 68	88.5	51.5	: -56	36.5	43.75	63		
S	ŀ	#2	55			-55.25			62.5		
T	1	#8	1 55	60.5	43.75	: -56	58.5	40	49.5	23.5	67 1
	t	#6	1 54	1 63	1 47	-51	46.5	38.5	49	25.5	61.5
P	1	#1	1 39.5	1 55	47.5	-54	49.5	38.5	48	23.75	60.75
A	i	# 7	40.5	; 55	47	-55.75	47.75	37.75	26	24.5	61.75
S	1	#3	1 41.5	1 53	1 25.5	-54.5	1 50.75	37	26.5	19.25	63.5 1
S	;	#9	40.5	1 53.5	1 26	-53	51.5	37	25	18.5	33.75
	1		}	:	1	1	1	1	;	}	: :
	!		1	† t	!	! !	:	1	1	;	! !
S	;		1	;	t i	1	!	t 1	; ;	:	: :
Ε	1	#5	41	: 59	24.5	-63.5	33.25	31.25	26	21	35 !
C	!	#6	: 41.5	59.5	1 24	: -63.25	1 38	: 6	26	19.5	35.25
8	1	#2	; 39	; 20	18.5	-64.5	37.75	1 6.25	27	; 21	35.5
N		#8	38.5	1 20.5	1 19	1 -65	: 39	6.75	27	-3.5	33 1
Ţ;	;	#1	1 -2		19.5	1 -66.25	38.75	6.5	27.5	-1.5	33.5 :
•	;	#3	-2.25					5.75	27	; -3	33 :
Р	;	#7	: -2							1 -3	32.75
A	•	#9	; -2								-10.5 (
S	1	π/	!	!		!	!	!		!	1
S	i		!	;				!		1	1

3/16" PLATE
Out of plane deflection at the center of panel i. referenced to the longitudinal straight line connecting the mid points of that panel's transverse stiffeners. See Figure 3-2 for the definition of D(MAX)iL.

	ŀ	PANEL	t t	1	i i	1	1	:	!	!	;	
	- }}	IEATED*	1D(MAX)1L	. ID(MAX)2L	(D(MAX)3L	!D(MAX)4L	(D(MAX)5L	(BCNAX)6L	1D(MAX)7L	18(XAX)01:	ID(MAX)9L)	i
	1			: :	! !	: 	!	; ¦	,	¦	,, ;	,
F	1	WELD	1 56	61	47	70.5	58.5	47	: 54	31	56 :	
I	ł	#5	62.5	; 93	1 45	1 66	32.5			; 54	59.5	i
R	1	#4	1 62	1 85.75	43.5	: -6	46.5	40	57.5	49.5	53 :	
S	-	#2	: 54	: 53.5	42.5	-6.5	52.75	41.5	1 58	44.75	52	
Ţ	ł	#8	1 54.75	1 51	43.5	-8.75	61.25	43.5	: 48	2.25	53 1	
	1	#6	1 52.5	: 58.5	46.5	· -6	56.25	53	1 48	8.75	1 54.5	į
Ρ	- 1	#1	: 50.75	1 55.25	49.5	-16.25	62.25	55.75	46.5	7.25	52.5	
A	ŀ	#7	1 51	1 55.5	1 49	1 -14.5	1 62	55.25	31.5	: 9	52.5	t L
S	ł	#3	1 51.5	1 55.25	1 35	1 -12.75	64.5	53	32.25	10	54.5	J
S	1	#9	1 51	1 57	: 35	-11.5	1 66	51.75	1 32	: 9	31.75	į
	1		}	1	1	!	!	!	:	Į Į	1 1	
	- {		:	1	i t	1	1	!	1	!	1	ŀ
S	1		† 1	1	1	!	!	;	!	!	1	
Ε	;	# 5	1 52	1 61.75	33.5	-19	50.25	46.75	33.5	10.75	34.5	i
C	!	#6	1 52.5	1 62	1 32	-19	55	23.5	33.75	11	: 34 :	
0	i	#2	1 51	1 22.5	1 28	-19.5	1 55.5	1 24	34	10.5	33.5	ŀ
N	1	#8	; 51	23	27.75	-21	55.5	1 24	: 34	-13.5	31.75	J
D	;	#1	10.5	1 20	28.5	-22	55.5	1 24	34.5	-11.5	31.5	į
	1	#3	1 10	1 23	1 2	-21	: 56	22.5	34.5	-13	31.5	
P	1	#7	1 9.25	22.5	2.25	1 -22.5	56.5	22.5	15	-13	31.25	:
Α	;	#9	1 10.5	1 23	1 2	1 -20.5	56.5	22.5	14	1 -16.5	-11.35	J
S	1		:	1	! !	1	1 1	:	1	!	ŀ	:
S	į		1	;	;	}	;	l i	;	;	; ;	

APPENDIX W

1/8" STIFFENED PLATE MID-PANEL DEFLECTION DATA D(MAX)iT AND D(MAX)iL

This appendix contains the mid-panel deflection data. D(MAX)iT and D(MAX)iL, for the 1/8" stiffened plate. The data is in tabular form. All deflection readings are in thousandths of an inch. See Figure 3-2 for the definition of D(MAX)iT and D(MAX)iL.

1/8" PLATE

Out of plane deflection at the center of panel i. referenced to the transverse straight line connecting the Mid points of that panel's longitudinal stiffeners. See Figure 3-2 for the definition of IMMAXII.

	FANEL HEATED*	 D(MAX)1T	 D(HAX)2T 	 D(HAY)3T !	D(MAX)4T	; !D(MAX)ET:	: :IN:MAX /6T:	(I)(MAX)?T	: IP/max.)8T 	IBK MAX /97 ''
F I R S T P A S S	#5 #4 #4 #6 #4 #8 #8 #3 #1 #7	69.5 75.5 93 94 96.5 96.5 93.5 126.5 127.5	4 : 4.5 4 : -5.5 -6.5 -8 -17.5 : -18	37 34 39.5 43.5 43.5 -6.5 -7	24 20.5 20 20.5 19.75 14.75 16.5	24.5 (25) 26.5 (28.75) 28.5 (32.25)	12 13 14.25 13.5 11 7.5 9.5	93.5 95.5 96 95.25 89 88 90 123	16 16 15 15.75 15.75 1-12 1 -13 1 -26.5	53.5 : 54.5 : 55.25 : 54.5 : 5
S E C O N	#5 #5 8600 After Danage #5	1 129.5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-19	-10.5	17.5		 -3	124.25	-16.5	: : : : : : : : : : : : : : : : : : :
P A S S	#4 #1 #7 	1 129.25 1 108 1 108	-20.5	-9	-9.5		-2.5	1 124	-16	-73.75 (-74.5 (-74.5 (
3 R D P A S	#1 #7	67.25				-55.5 -58				-74 : -74.5 : : : : : : : : : : : : : : : : : : :
4 T H P A S S	; ; ; ; #7 ; #1	24.5	-23		-8.5 -8.75			67.75	-11.75	

PANEL WS WAS HEATED. PANELS W9 AND W4 WERE AFFECTED

1.'8" FLATE

Out of plane deflection at the center of panel i. referenced to the longitudinal straight line connecting the Mid points of that panel's transverse stiffeners. See Figure 3-2 for the definition of D-MAX/LL.

PANEL HEATED# 	; D(HAX)1L 	! D(HAX)2L 	! :D(HAX)3L !	 D(hax)4L 	: (D(MAX)5L !	! D/ MAX >6L 	: D(MAX)7E 	; :D(MAX)8L ;======	 [] (
#5 #4 #6 #6 #2 #8 #3 #1 #7 #9	1 55 1 74.75 1 76 1 78 1 79.25 1 76.5 1 118.5 1 119.5	-17 -16.5 -17.5 -27 -26.75 -27.75 -35.5 -35.75	21 18.75 24.5 28.25 28.25 28.25 -18.25 -19.25	6.25 6.25 6.5 6.25 6.25 6 0	6.25 8 8 8 8 8 12 5 12 5 12 5 1	0.5 : 3.5 : 3.75 : 3.25 : 0.75 : 3 : -2 :	77.5 78.75 78.5 79.25 73 71.75 74.5 113.75	-10 -10.5 -10.75 -10 -37.5 -38 -38.5 -49.5	41 42 45 43.75 43.75 42.75 40.75 43.5
#1	: :	-37 (-38.5 (-22.75 -21.5 -22.25	1.75 -25 -24	-71.5 -71.5 -71 -65.5 -68.75 -71	-14.75 -17 -15.25	115.25 114 114.5	-38.5 -37.5 -38.25	-83.5 -84
#1 #7	60.75 59.75				-7 4.2 5			-37.5 -33.5	
W7 W1	18	-39		-23.5 -23.5	-77.25 : -77		59.5	-33.25	

PANEL #5 WAS HEATED. PANELS #9 AND #4 WERE AFFECTED

APPENDIX X

AFFECT ON D(MAX)iT AND D(MAX)iL OF LINE HEATING EACH PANEL ON THE 3/16" STIFFENED PLATE

There are two types of comparisons made in this appendix:

- 1. the affect on D(MAX)iT and D(MAX)iL of line heating each of the panels, and
- each of the panels, andthe affect on D(MAX) of all other panels when line heating just one panel.

All data in the tables are in thousandths on an inch.



A. 3/16" STIFFENED PLATE. FIRST PASS

E COM POSSESSE CONTRACTOR DODGE CONTRACTOR DODGE CONTRACTOR DESCRIPTION OF THE PROPERTY OF THE

PANEL #1

 The affect on D(MAX)1T and D(MAX)1L of line heating all other panels.

TRANSVERSE	LONGITUDINAL	
1-14.5 -13 1	 -1.75	
-3.75 8.25 -1	-0.5 6.5 -2.25	
1 0 -1	0.25 0.75 -0.5	

2. The affect on D(MAX) of all other panels by heating panel #1

TRANSVERSE	LONGITUDINAL	
1-14.5 -8 0.5	1-1.75 1-3.25 1 3 1	
-3 3 0	-10.3 6 2.75	
-1	-1.5 -1.5 -2	
' ' ' '	,,	

PANEL #2

 The affect on D(MAX)2T and D(MAX)2L of line heating all other panels.

TRANSVERSE	LONGITUDINAL
 -8 -26 -2	1-3.25 -32.3 -0.25
-8.25 33.3 2.5	1-7.25 32 7.5
0 -2 0.5	0.25 -2.5 1.75

TRANSVERSE	LONGITUDINAL
-13 -26 -9	
0.75 10.5 2.75	-0.5 6.25 1.5
-0.5 -4 -2	0.5 (-4.75) -1)

PANEL #3

1. The affect on D(MAX)3T and D(MAX)3L of line heating all other panels.

TRANSVERSE	LONGITUDINAL
0.5 -9 -21.5	3 -1 -14
	 -1.5 -2 3
(-0.5 1.25 0.5 	-0.5 1 0

2. The affect on D(MAX) of all other panels by heating panel #3

TRANSVERSE	LONGITUDINAL		
1 -2 -21.5			
1.25 3 -0.75	1.75 2.5 -2.25		
0.5 0.75 1.75	0.75 1 2		
	· · · · ·		

FANEL #4

1. The affect on $B(\,\text{MAX}\,)4T$ and $\,\,D(\,\text{MAX}\,)4L$ of line heating all other panels.

TRANSVERSE	LONGITUDINAL	
 -3 0.75 1.25		
-102 -12.3 5	-72 -4.5 2.75	
(-1.75 -0.75 1.5	1.75 -2.25 1.25	

TRANSVERSE	LONGITUDINAL		
-3.75 -8.25 -0.5	-0.5 -7.25 -1	.5 :	
-102 3.25 1.75	-72 14 -0	.5 :	
-1 -5.5 -6	1.5 -4.5 -6.	25 Î	

PANEL #5

1. The affect on D(MAX)ST and D(MAX)SL of line heating all other panels.

TRANSVERSE		
3 10.5 3	2.5 2.5 1	
3.25 -29.8 -12	14 -26 -5	
 -1.75 11.5 0.75 	-0.25	

2. The affect on D(MAX) of all other panels by heating panel #5

TRANSVER					NAL
1 8.25 133.25	-3	1 6.	5	32	 -2
 -12.3 -29.8 	1-11.5	1 -4.	5	-26	6.5
1 3.5 23	3.5 (1	2	23	3.25

PANEL #6

1. The affect on D(MAX)6T and D(MAX)6L of line heating all other panels.

TRANSVERSE	LONGITUDINAL	
0 2.75 -0.75	2.75 1.5 -2.25	
1.75 -11.5 -1.5	1 -0.5 -6.5 9.5	
1-0.75 -6.5 0	-0.5 2 -1.25	

TRANSVERSE	LONGITUDINAL
-1 2.5 3.25	 -2.25
5 -12 -1.5	1 2.75 -5 9.5
-0.5 2 -5.5	0 6.5 1.5

1. The affect on D(MAX)7T and D(MAX)7L of line heating all other panels.

TRANSVERSE		LONGITUDINAL				
-1	-0.5	0.5		-1.5	0.5	 0.75
-1	3.5	-0.5		1.5	2	0
-22	-13	-1.5	1	-15	-10	-0.25

2. The affect on B(MAX) of all other panels by heating panel #7

TRANSVERSE	LONGITUDINAL	
		- 1
1 0 -0.5	1 0.25 0.25 -0.5	ŧ
		- ;
1-1.75 -1.75 -0.75	1 1.75 1-0.25 1 -0.5	ŀ
		-
-22 -1.75 1	-15 1.75 0	1
		- ;

FANEL #8

1. The affect on D(MAX)8T and D(MAX)8L of line heating all other panels.

TRANSVERSE	LONGITUDINAL
0 -4 0.75	 -1.5 -4.75 1
-5.5 23 2	-4.5 23 6.5
 -1.75	

TRANSVERSE	LONGITUDINAL			
0 -2 1.25	0.75 -2.5 1			
 -0.75	1-2.25 8.5 2			
	[
-13 -41.5 1	1 -10 (-42.5) 1 (

PANEL #9

1. The affect on D(MAX)9T and D(MAX)9L of line heatino all other panels.

TRANSVERSE	LONGITUDINAL
-0.75 -2 1.75	-2 -1 2
-6 3.5 -5.5 	
1 1 -29.8	0 1 1 1-22.8 1

2. The affect on D(MAX) of all other panels by heating panel #9

TRANSVERSE	LONGITUDINAL
 -1 0.5 0.5 	 -0.5 1.75 0
1.5 0.75 0	1.25 1.5 -1.25
-1.5 -5.25 -29.8 	-0.25

B. 3/16" STIFFENED PLATE. SECOND PASS

PANEL #1

1. The affect on D(MAX)1T and D(MAX)i! of line heating all other panels.

TRANSVERSE	LONGITUDINAL
1-40.5 -2.5 0.25	1-40.5 -1.5 -0.5
{;	
1 N/A -0.5 0.5	N/A 0.5 0.5
	(
1-0.25 -0.5 0	1-0.75 0 1.25

2. The affect on D(MAX) of all other panels by heating panel #1

TRANSVERSE	LONGITUDINAL
 -40.5	 -40.5
-1.25	1 -1 0 0
0.5 2 0.5	1 0.5 2 -0.25

PANEL #2

1. The affect on D(MAX)2T and D(MAX)2L of line heating all other panels.

TRANSVERSE LONGITUDI		. –		
1 -3.5 1-39.5 1 3.25 1	1 -3	1-39.5	 3 	
N/A 6 0.5	I N/A	5.75	0.25	
-0.25 0.5 -0.5	-0.5	0.5	0.5	

TRANSVERSE	LONGITUDINAL			
 -2.5 -39.5 -5.5	-1.5 -39.5 -4			
-1.25 -0.25 0.25	 -0.5 0.5 0.5			
1 1.5 0.25	0.25 -0.5 -0.5			

THE PARTY OF THE PROPERTY OF THE PARTY OF TH

1. The affect on D(MAX)3T and D(MAX)3L of line heating all other panels.

TRANSVERSE	LONGITUDINAL		
0.5 -5.5 -27.5	0.75 -4 -26.5		
N/A -2.5 -0.5	 N/A -2.5 -1.5 		
1 0.5 -1	0.25 -0.25 -0.25		

2. The affect on D(MAX) of all other panels by heating panel #3

TRANSVERSE		LONGITUDINAL				
-0.25	3.25	1-27.5	:	-0.5	3	-26.5
0.75	0.25	1-0.75	:	1	0.5	: : -1.5 :
-0.5	-1.5	0.5		0	-1.5	. 0
;	;	!		;	i	;

PANEL #4

1. The affect on B(M4X)4T and B(M4L) of of line heating all other panels.

TI						łAL .
(-1.25	-1.25	0.75		-1	-0.5	1
N/A	-8	 0.25 	!	N/A	-5.5	0 1
1 -0.5	-0.5	0.5		-1.5	-1.5	2

TRANSVERSE		LOì	ACITUDI)	NAL
-		!	 	
		¦	, 	
	!	!	1	
		; - ;		
-	!			

PANEL #5

1. The affect on D(MAX)ST and D(MAX)SL of line heating all other panels.

TRANSVERSE	LONGITUDINAL
1-0.25 1-0.25 1 0.25 1	1 0 1 0.5 1 0.5 1
N/A -18.3 4.75	N/A -15.8 4.75
1 1.5 1.25 -1	1 0.5 1 0 1 0 1
	[]]

2. The affect on D(MAX) of all other panels by heating panel #5

TANDAR STATES FRACTOR SECTION STATES

TRANSVERSE	LONGITUDINAL
1 -0.5 1 6 1 -2.5 1	0.5 5.75 -2.5
[[]
-8 -18.3 -5.5	1 -5.5 -15.8 -4
1 0.5 1 0.25 1 0.5 1	1.75 1.75 1.25
[]	{}

FANEL #6

1. The affect on $B(MAX)\delta T$ and $B(MAX)\delta L$ of line heating all other panels.

TRANSVERSE	— · · · · - ·	TUDINAL
1-0.25 0.25 -0.75	1 0 1	0.5 -1.5
 N/A	1 N/A 1	-4 -23.3
1 0.75 0.5 -1	0 1	0 0

TRANSVERSE	LONGITUDINAL		
1 0.5 1 0.5 1 -0.5 1	1111		
0.25 4.75 -25.3	0 4.75 -23.3		
0 -1.5 0.25	1 0.25 0.25 -0.5		

PANEL #7

1. The affect on D(MAX)7T and D(MAX)7L of line heating all other panels.

TF				
0.5	1	-0.5	1 0.5 1 0.25	0 1
N/A	0.5	0	N/A 1.75	0.25
-19.5 	0 :	0	!-19.5 O	-1

2. The affect on D(MAX) of all other panels by heating panel #7

TI			, LO1		
0.25	-0.25	1 1	1-0.75	-0.5	0.25
-0.5	1.5	0.75	: -1.5	0.5	
-19.5	0	1-0.25	-19 . 5	0	-0.25

PANEL #8

1. The affect on D(MAX)8T and D(MAX)8L of line heating all other panels.

TRANSVERSE	LONGITUDINAL
(
2 1.5 -1.5	2 -0.5 -1.5
 N/A	N/A 1.75 0.25
0 -24.5 -2.5	0 -24 -3.5

	- ;
1 -0.5 1 0.5 1 0.5 1 1 0 1 0.5 1-0.2	
	•
-0.5 1.25 0.5 -1.5 0	
0 -24.5 -2.5 0 -24 -1.7	
0 -24.5 -2.5 0 -24 -1.5	

PANEL #9

 The affect on D(MAX)9T and D(MAX)9L of line heating all other panels.

TRANSVERSE	LONGITUDINAL
0.5 0.25 -0.5	-0.25 -0.5 0
N/A 0.5 0.25	 N/A 1.25 -0.5
1-0.25 -2.5 -43.3	-0.25 -1.75 -42.6

2. The affect on D(MAX) of all other panels by heating panel #9

	NSVERSE	==:	LONGITUDINAL		
0 1	-0.5 -1	1.25	0.5	1-0.25	
i 0.5 i	-0.5 -1		0	0	
•	¦¦ -2.5 ¦-43.8 ¦	-1	-3.5	1-42.6 1	
}		;	¦	\	

APPENDIX Y

AFFECT ON D(MAX)iT AND D(MAX)iL OF LINE HEATING EACH PANEL ON THE 1/8" STIFFENED PLATE

There are two types of comparisons made in this appendix:

- the affect on D(MAX)iT and D(MAX)iL of line heating each of the panels. and
- each of the panels, andthe affect on D(MAX) of all other panels when line heating just one panel.

All data in the tables are in thousandths on an inch.

A. 1/8" STIFFENED PLATE. FIRST PASS

PANEL #1

 The affect on D(MAX)1T and D(MAX)1L of line heating all other panels.

. 1						NAL .
33	2.5	-2.5		42	2	 -2.75
17.5	6	1		19.75	6.25	1.25
. 0	-0.5	: 0		1	1.25	0.5
			i	:	;	!

2. The affect on D(MAX) of all other panels by heating panel #1

TRANSVERSE		ı	LONGITUDINAL				
1 33	-9.5	-0.5		42	l-7.75	-1	i
-5	8.5	-3.5		-6	{ 8.5	2.25	1
12	-1	-2.5		2.75	: -0.5	-2	•
!	i	; ;			¦		i

PANEL #2

1. The affect on D(MAX)2T and D(MAX)2L of line heating all other panels.

TRANSVERSE			LONGITUDINAL		
1 -9.5	9.5	-1.5 	1-7.75 1	-9.5	-1
0.5	-3.5	-0.5	1 0.5 ;	-3	-1 }
-0.5	-1	•	1-0.25	0.25	0.5

TRANSIJERSE	LONGITUTINAL		
1 2.5 -9.5 4	2 -9.5 3.75		
0 2.25 1.25	0 1.75 0.25		
 -0.75	 0.75 0.75 -1.25 		

PANEL #3

1. The affect on D(MAX)3T and D(MAX)3L of line heating all other panels.

 -0.5	•	
	6.5	1
1 -3 4.5 5.5	.75	:
-0.5 -0.5 1.5 0.25 0	1	:

2. The affect on D(MAX) of all other panels by heating panel #3

TRANSVERSE	LONGITUDINAL
 -2.5 -1.5 -49	 -2.75
1-0.75 3.75 -2.5	-0.25 4.25 -2.5
	 -1.25

PANEL #4

 The affect on D(MAX)4T and D(MAX)4L of line heating all other panels.

TRANSVERSE	LONGITUDINAL		
 -5 0 -0.75	-6		
-3.5 -10.3 -0.5	1 0.25 -8.5 0.25		
1.75 0.5 -0.25	0.25 -0.25 -0.5		

TRANSVERSE	LONGITUDINAL
1 18.5 1 0.5 1 -3 1	119.75 0.5 1-2.25
-3.5 0.5 -1	0.25 1.5 0.5
2 0 1 1 1	11.25 -0.5 1

1. The affect on D(MAX)ST and D(MAX)SL of line heating all other panels.

TRANSVERSE	LONGITUDINAL
8.5 2.25 3.75	8.5 1.75 4.25
0.5 -45.3 1.5	1.5 -43 2.25
 7 -0.25 4.75 	7.75 0.25 5.25

2. The affect on D(MAX) of all other panels by heating panel #5

TRANSVERSE	LONGITUDINAL			
6 1 -3.5 1 4.5 1	1 6.25 1 -3 1 5 1			
 -10.3 -45.3 -14.5 	 -8.5 -43 -12.5 			
8.5 -1 4	9 1 -1.5 1 4 1			

FANEL #6

1. The affect on D(M6X)6T and D(M6L) of of line heating all other panels.

TRANSVERSE	LONGITUDINA	L
	-	
-3.5 1.25 -2.5	1 2.25 0.25	
	1 0.5 (-12.5)	
	-	
2 1-0.75 -5	-5 -0.5	

TRANSVERSE	LONGITUDINAL		
 1 -0.5 5.5 	1.25 1 5.75	1	
-0.5 1.5 1	0.25 2.25 3	ļ	
0.5 -1 1.5	-0.25 -0.25 3 	ì	

. The affect on D(MAX)7T and D(MAX)7L of line heating all other panels.

TRANSVERSE	LONGITUDINAL
2 -0.75 -1	2.75 0.75 -1.25
	1.25 9 -0.25
33 -6.25 -1	139.25 1-6.25 0

. The affect on D(MAX) of all other panels by heating panel #7

TRANSVERSE	LUNGITUDINAL	LONGITUDINAL		
1 -0.5 -0.5	1 -0.25 0.25	;		
1.75 7 2	0.25 7.75 -5	į		
33 -13.5 3.5	39.25 -11 2.75 	i		

PANEL #8

. The affect on D(MAX)8T and D(MAX)8L of line heating all other panels.

TRANSVERSE		LUNGITUDINAL
-1 0.75	0 1	-0.5 0.75 -0.5
0 -1	-1	-0.5 -1.5 -0.25
1-13.5 1-27.8	-6	-11 -27.5 -4.5

TRANSVERSE	LONGITUDINAL		
; -0.5; -1; -0.5;	1.25 0.25 0		
 0.5 -0.25 -0.75 	 -0.25		
-6.25 -27.8 -0.75 	-6.25 -27.5 -0.75 		

 The affect on D(MAX)9T and D(MAX)9L of line heating all other panels.

TRANSVERSE	LONGITUDINAL		
-2.5 -0.75 -0.5	-2 -1.25 -2.5 -2 -1.25 -2.5		
1 4 1.5	1 4 3 1		
3.5 -0.75 -15	2.75 -0.75 -11.3		

2. The affect on D(MAX) of all other panels by heating panel #9

TRANSVERSE		_	LONGITUDINAL		
0 1	0 1	1.5	0.5 0.5		
 -0.25	4.75	-5 }	-0.5 5.25 -5.		
 -1	-6 1		0 -4.5 -11.		

THE PERSON NAMED OF PARTY AND PARTY OF THE PERSON OF THE P

B. 1/8" STIFFENED PLATE. SECOND PASS

PANEL #1

1. The affect on D(MAX)1T and D(MAX)1L of line heating panels #5. #4. #1, and #7 a second pass.

TRANSVERSE	LONGITUDINAL		
1-21.3 1	 -19.5		
-21.5	[
1 -1.5 3.25	1-1.5 2.5		
	 -1.25		

2. The affect on D(MAX) of all other panels by heating panel #1

TRANSVERSE	LONGITUDINAL		
1-21.3 0 0	 -19.5 1 -0.75		
0.75 -3.5 1.75	1 -3.25 1.75		
1 -0.75 -0.75	 0.5 -0.75 -0.5		

PANEL #2

 The affect on D(MAX)2T and D(MAX)2L of line heating panels #5, #4, #1, and #7 a second pass.

TRANSVERSE	LONGITUDINAL
0	1
-1.5 -1	-1.5 -1.75
1 1	0.5
11	

PANEL #3

The affect on D(MAX)3T and D(MAX)3L of line heating panels #5,
 #4, #1, and #7 a second pass.

TRANSVERSE	LONGITUDINAL
: 0: : :	1-0.75
[
1.5 -5	1 1.25 1-4.75 1
1-0.25	: 0.25 : : :
	203

PANEL #4

The affect on D(MAX)4T and D(MAX)4E of line heating panels #5.
 #4, #1. and #7 a second pass.

TRANSVERSE	LONGITUDINAL		
10.75	1 1 1 1		
1-27.8 1.25	1-26.8 1 2 1 1		
1 0 1 1	1-0.25		

2. The affect on D(MAX) of all other panels by heating panel #4

TRANSVERSE		LONGITUDINAL			
-	-1.5	1.5	-1.5	-1.5	1.25
1-27.8	5.5	-1.25 	1-26.8	5.5	 -2.25
	1.25	1-0.25	-1.25	1	 -1.5

PANEL #5

and production streets in the second of the second of the second of the second seconds the second of

1. The affect on D(MAX)5T and D(MAX)5L of line heating panels #5. #4, #1, and #7 a second pass.

TRANSVERSE	LONGITUDINAL
	-3.25
 5.5 -105 	5.5 -105
1 -2.5	

TRANSVERSE	LONGITUDINAL	
3.25 -1 -5	2.5 [-1.75 [-4.75]	
1.25 -105 -7.5	2 -105 -7.25	
2.25 16 -114	1.5 15.5 -114	
1		

PANEL #6

1. The affect on $\mathbb{P}(\text{MAX})\delta T$ and $\mathbb{P}(\text{MAX})\delta L$ of line heating panels #5. #4. #1. and #7 a second pass.

TRANSVERSE	LONGITUDINAL	
1.75	1.75	
1-1.25 -7.5	1-2.25 1-7.25 1	
	0.25	

PANEL #7

1. The affect on D(MAX)7T and D(MAX)7L of line heating panels #5. #4, #1, and #7 a second pass.

TRANSVERSE	LONGITUDINAL	
1 1	1 0.5 1 1 1	
-1.25 2.25	[-1.25 1.5	
: -10 : :	1-9.5	

2. The affect on D(MAX) of all other panels by heating panel #7

TRANSVERSE	LONGITUDINAL	
0 1 1-0.25	-1.25 0.5 0.25	
 0 -2.5 -0.5 	 -0.25 -2.25 0.25 	
-10 0.5 0	-9.5 1.25 0.75 	

FANEL #8

1. The affect on D(MAX)8T and D(MAX)8L of line heating panels #5, #4, #1, and #7 a second pass.

TRANSVERSE	LONGITUDINAL	
1-0.75	1-0.75	
	[]	
1 1.25 16	1 1 15.5	
1 0.5 1 1 1	1 1.25 1	
	[[[

PANEL #9

1. The affect on D(MAX)9T and D(MAX)9L of line heating panels #5. #4, #1, and #7 a second pass.

TRANSVERSE	LONGITUDINAL	
1-0.75	1 -0.5 1 1 1	
1-0.25 -114	-1.5 114	
1 0 1 1 1	10.75	
[]		

C. 1/8" STIFFENED PLATE. THIRD FASS

PANEL #1

2. The affect on D(MAX) of all other panels by heating panel #1

TRANSVERSE	LONGITUDINAL	
-40.7 -3.5 0.75	1-39.5 -3 1	
0 -3 1.75	 0.25 -3.25 1 	
-0.25 -0.25 0.5	0 -0.5 0	
	(

PANEL #7

TI	RANSVER	SE	LONGITUDINAL
{	!		
1 -25	1 0	1 0.5 1	
•	•	!	·
		1 -0.5	
•	•		
		: -0.5 :	

D. 1/8" STIFFENED PLATE. FOURTH PASS

STATES OF THE PROPERTY OF THE PARTY OF THE PROPERTY OF THE PRO

FANEL #7

2. The affect on D(MAX) of panels #4, #5, #7, and #8 by heating panel #7.

TRANSVERSE	LONGITUDINAL	
-0.5 -1		
 -25.8	 -26 0.25 	

PANEL #1

2. The affect on D(MAX) of panels #1, #2, #4, and #5 by heating panel #1.

TRANSVERSE	LONGITUDINAL
-43 0	 -41.8
 -0.25	0 0.25

REFERENCES

- 1. Masubuchi. K.. Analysis of Welded Structures. International Series on Materials Science and Technology, vol. 33. Oxford: Pergamon Press. 1980.
- 2. Pattee. H.E.. Evans. R.M.. Monroe. R., "Flame Straightening and its Effect on Base Metal Properties", Battelle Memorial Institute, Columbus. Ohio, SSC-198, August 1969.
- 3. Holt. R.E.. "Flame Straightening Basics", Welding Journal, vol. 44, September 1965, pp. 49 52.
- 4. Holt. R.E., "Primary Concepts for Flame Bending", Welding Journal. vol. 50, June 1971, pp. 416 424.
- 5. Anonymous. "Line Heating", The National Shipbuilding Research Program, U.S. Department of Transportation, Maritime Administration in Cooperation with Todd Pacific Shipyards Corporation, November 1982.
- 6. Borzecki, T., Rosochowicz, K., "An Effective Method of Straightening Thin-Walled Superstructures", The 2nd International Symposium on Practical Design in Shipbuilding, Tokyo and Seoul, 1983, pp. 389 396.
- 7. Papazoglou, V.J., Masubuchi, K., "Development of Analytical and Empirical Systems For Parametric Studies of Design and Fabrication of Welded Structures", Final Report Prepared Under Contract No. N00014-75-C-0469, Nr 031-773, submitted to The Office of Naval Research, November 1977.

- 8. Ractliffe, A.T., "The Basis and Essentials of Thermal Residual Distortion in Steel Structures", The Royal Institution of Naval Architects, 1983, pp. 217 225.
- 9. Anonymous. "Flame Buckled this Steel ... and Flame Straightened it!, Part I", Welding Engineer, vol. 44, 1959, pp. 40 -43.
- 10. Walsh, R.A., "Investigation of Distortion Removal in Welded Structures", S.M. Thesis, Department of Ocean Engineering, M.I.T., Cambridge, MA., May 1969.
- 11. Duffy, D.K., "Distortion Removal in Structural Weldments", S.M. Thesis, Department of Ocean Engineering, M.I.T., Cambridge, MA., May 1970.
- 12. Johnson, E.K., "Study of Flame Heating of Steel Plate", S.M. Thesis, Department of Ocean Engineering, M.I.T., Cambridge, MA., May 1971.

- 13. Taniguchi, C., "Out-Of-Plane Distortion Caused by Fillet Welds in Aluminum", S.M. Thesis, Department of Ocean Engineering, M.I.T., Cambridge, MA., September 1972.
- 14. Henry, R.W.. "Reduction of Out-Of-Plane Distortion in Fillet Welded High Strength Aluminum", S.M. Thesis, Department of Ocean Engineering, M.I.T., Cambridge, MA., May 1974.
- 15. Pattee. H.E., Evans, R.M., Monroe, R.E., "Experimental Flame and Mechanical Straightening and its Effects on Base Metal Properties", Battelle Memorial Institute, Project SR-185, Columbus, Ohio, July 1969.
- 16. Iwamura, Y., Rybicki, E.R., "A Transient Elastic-Plastic Thermal Stress Analysis of Flame Forming", <u>Transactions of ASME</u>, vol. 95, February 1973, pp. 163 171.
- 17. Watanabe, M., Satoh, K., "Effect of Welding Conditions on the Shrinkage Distortion in Welded Structures", Welding Research Supplement, August 1961, pp. 377 - 384.
- 18. Muraki, T., Bryan, J.J., Masubuchi, K., "Analysis of Thermal Stresses and Metal Movement During Welding, Part I Analytical Study", <u>Journal of Engineering Materials and Technology</u>, January 1975, pp. 81 84.

- 19. Masubuchi, K., "Models of Stresses and Deformation Due to Welding--A Review", <u>Journal of Metals</u>, vol. 33, December 1981, pp. 19-23.
- 20. Papazoglou, V.J., Masubuchi, K., "Numerical Analysis of Thermal Stresses During Welding Including Phase Transformation Effects", <u>Journal of Pressure Vessel Technology</u>, vol. 104, August 1982, pp. 198 203.
- 21. Papazoglou, V.J., Masubuchi, K., Goncalves, E., Imakita, A., "Residual Stresses Due to Welding: Computer-Aided Analysis of Their Formation and Consequences", <u>SNAME</u>, November 1982.
- 22. Agapakis, J.E., Papazoglou, V.J., Imakita, A., Masubuchi, K., "Study of Residual Stresses and Distortion in Structural Weldments in High-Strength Steels", Final Report Prepared under Contract N00014-75-0469, submitted to The Office of Naval Research, November 1982.
- 23. Agapakis, J.E., Masubuchi, K., "Analytical Modeling of Thermal Stress Relieving in Stainless and High Strength Steel Weldments", Welding Research Supplement, June 1984, pp. 187-196.
- 24. Tsai, C.L., "Modeling and Control of Out-Of-Plane Welding Distortion in Fabricated Structure Members", Publisher and date unknown.

- 25. Shin. D.B., "Finite Element Analysis of Out-Of-Plane Distortion of Welded Panel Structures", S.M. Thesis, Department of Ocean Engineering, M.I.T., Cambridge, MA., May 1972.
- 26. Masubuchi. K., Imakita, A., Miyachi, H., Miyake, M., "Development of an Intelligent System for Flame Straightening Panel Structures". Paper to be Presented at The National Shipbuilding Research Program, Ship Production Symposium, 1987.
- 27. Ingerson, F.E., Conversation on the welding sequence to use while welding the 1/8" stiffened plate, Middlesex Welding Supply, Cambridge, MA, January 1987.
- 28. Masubuchi, K., Terai, K., "Future Trends of Materials and Welding Technology for Marine Structures", SNAME, June 1976.